

EMP Theoretical Notes

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Extrapolating Transient Multipole Fields

By

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The first part of the document discusses the importance of maintaining accurate records of all transactions. It emphasizes that every entry should be supported by a valid receipt or invoice. This not only helps in tracking expenses but also ensures compliance with tax regulations.

In the second section, the author outlines the various methods used to collect and analyze data. These include direct observation, interviews, and the use of specialized software tools. Each method has its own strengths and limitations, and the choice of which to use depends on the specific requirements of the study.

The third section provides a detailed overview of the results obtained from the data collection process. It highlights key findings and trends, such as the significant increase in sales during the holiday season and the growing importance of digital marketing channels.

Finally, the document concludes with a series of recommendations for future research and business strategy. It suggests that further exploration into the impact of social media on consumer behavior would be a valuable area of study. Additionally, it advises businesses to continue investing in technology to streamline their operations and improve customer service.

ABSTRACT

An improved method of extrapolating transient EM fields has been developed and a computer code has been written to implement the technique. This paper contains a summary of the theory and a listing and description of the computer code.

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I. INTRODUCTION

The field extrapolation method reported here is a considerable improvement over the previously used method.¹ The spherical vector components are treated directly, using only E_{θ} as input rather than transforming to rectangular components, extrapolating, and then transforming back again. The new method is much simpler and is faster to perform numerically. In addition, the numerical method of performing the convolution integrals has been improved to make it faster and more accurate. Program M, the new computer method described in Sec. IV, requires computer time linearly proportional to the number of time points treated, whereas the old method used computer time proportional to the square of the number of time points.

¹ D. D. Babb and K. D. Granzow, Extrapolating Electromagnetic Fields From Values in a Spherical Region, Sec. II, WL-TR-64-179, Air Force Weapons Laboratory, 1965.(EMP Theoretical Note 52).

II. ANALYSIS

The electromagnetic fields to be extrapolated are known within and on the surface of a sphere whose center lies in an infinitely conducting horizontal plane. The field possesses azimuthal symmetry about the vertical axis and is equal to zero at time equal to zero. The problem is to find the field as a function of time in the upper half space outside the sphere. The field components are given for any r by the following equations²:

$$E_r = - \sum_{\ell=1}^{\infty} \sqrt{\frac{\ell(\ell+1)}{r}} \Xi_{\ell}(r) a_{\ell}(t^*) \bar{P}_{\ell}(\cos \theta) \quad (1)$$

$$E_{\theta} = \sum_{\ell=1}^{\infty} \Lambda_{\ell}(r) a_{\ell}(t^*) \bar{P}_{\ell}^1(\cos \theta) \quad (2)$$

$$B_{\phi} = \sum_{\ell=1}^{\infty} \frac{1}{c} \frac{\partial}{\partial t^*} \Xi_{\ell}(r) a_{\ell}(t^*) \bar{P}_{\ell}^1(\cos \theta) \quad (3)$$

where only odd values of ℓ are needed in the summations for the assumed symmetry (the analysis will include both even and odd terms for the sake of generality). The functions \bar{P}_{ℓ} are normalized Legendre polynomials and \bar{P}_{ℓ}^1 are the normalized associated Legendre polynomials of the first kind;

² K. D. Granzow, Transient Spherical Waves, EMP Theoretical Note XXIV, Dec. 1, 1966 (also published as "Time-Domain Treatment of a Spherical Boundary-Value Problem," Journal of Applied Physics, Vol. 39, No. 7, June 1968, P. 3435). The equations here are the ϕ -independent part ($m=0$) of Eqs. 2, 3, and 6 of the reference.

t^* is retarded time defined as $t^* = t - r/c$; Λ_ℓ and Ξ_ℓ are differential operators given by

$$\Xi_\ell(r) = \sum_{j=0}^{\ell} \frac{\mu_{\ell j}}{r^{j+1} c^{\ell-j}} \frac{\partial^{\ell-j}}{\partial t^{*\ell-j}}$$

$$\Lambda_\ell(r) = \sum_{j=0}^{\ell+1} \frac{\nu_{\ell j}}{r^{j+1} c^{\ell+1-j}} \frac{\partial^{\ell+1-j}}{\partial t^{*\ell+1-j}}$$

$$\mu_{\ell j} = \frac{\prod_{k=0}^j (\ell+k)(\ell-k+1)}{\ell(\ell+1) 2^j j!}, \quad j=0, 1, \dots, \ell$$

$$\nu_{\ell j} = \mu_{\ell j} \frac{\ell(\ell+1) + j(j-1)}{\ell(\ell+1) - j(j-1)}, \quad j=0, 1, \dots, \ell, \quad \nu_{\ell, \ell+1} = \nu_{\ell \ell}$$

The field component E_θ is given at $r = R$ by

$$E_\theta(R, t^*) = \sum_{\ell=1}^{\infty} A_\ell(t^*) \bar{P}_\ell^1(\cos \theta) \quad (4)$$

Upon equating the coefficients of Eqs. 2 and 4, one can express the unknown coefficients $a_\ell(t^*)$ in terms of the known coefficients $A_\ell(t^*)$

$$\Lambda_\ell(R) a_\ell(t^*) = A_\ell(t^*) \quad (5)$$

It is convenient to express the above coefficients in terms of a dimensionless time variable $\tau = ct^*/R$. The operator $\Lambda_\ell(R)$ now becomes

$$\Lambda_\ell(R) = \frac{1}{R^{\ell+2}} \sum_{j=0}^{\ell+1} \nu_{\ell j} \frac{\partial^{\ell+1-j}}{\partial \tau^{\ell+1-j}}$$

Redefine the coefficients

$$b_{\ell}(\tau) = a_{\ell} \left(\frac{\tau R}{c} \right)$$

$$B_{\ell}(\tau) = A_{\ell} \left(\frac{\tau R}{c} \right)$$

Equation 5, expressed in terms of τ , becomes

$$\Lambda_{\ell}(R) b_{\ell}(\tau) = B_{\ell}(\tau) \tag{6}$$

Equation 6 is a differential equation whose solution will be found with the aid of a Green's function.³ The problem now becomes one of finding the Green's function that will satisfy the following equation:

$$\Lambda_{\ell}(R) G_{\ell}(\tau, \tau') = \delta(\tau - \tau'), \quad \tau' > 0 \tag{7}$$

with the initial condition

$$G_{\ell}^{(k)}(0, \tau') = 0, \quad k=0, 1, 2, \dots, \ell$$

The first step is to solve the homogeneous case. This involves finding the roots of the auxiliary equation. The roots of the resulting polynomials are given in the appendix of Ref. 2 as the roots of $\lambda_{\ell}(z) = 0$. If ℓ is even, there is one real root, $p_{\ell 0}$, and the rest are complex, $p_{\ell n} \pm iq_{\ell n}$, where $n = 1, 2, 3, \dots, m$; $m = \ell/2$ for ℓ even; $m = (\ell+1)/2$ for ℓ odd. If ℓ is odd, there is no real root.

³ The solution given here parallels the solution of the equation $\Xi_{\ell}(r_0)$ $\alpha_{\Xi}(\ell, m, t^*) = \beta_{\Xi}(\ell, m, t^*)$ given by Granzow in Multipole Theory in the Time Domain, EMP Theoretical Note VII, March 1965 (also Journal of Mathematical Physics, Vol. 7, 1966, p. 634), and in Ref. 1.

Let $H_\ell(\tau, \tau')$ be defined as $G_\ell(\tau, \tau')/R^{\ell+2}$, then H_ℓ can be expressed as a linear combination of exponentials multiplying sines and cosines with coefficients α_ℓ , $\beta_{\ell n}$, and $\gamma_{\ell n}$ yet to be determined.

$$H_\ell(\tau, \tau') = \alpha_\ell e^{p_{\ell 0}(\tau-\tau')} + \sum_{n=1}^m e^{p_{\ell n}(\tau-\tau')} \left[\beta_{\ell n} \sin q_{\ell n}(\tau-\tau') + \gamma_{\ell n} \cos q_{\ell n}(\tau-\tau') \right] \quad (8)$$

In order to apply the boundary conditions, the first ℓ derivatives of Eq. 8 are needed.

$$\begin{aligned} \frac{d^k}{d\tau^k} H_\ell(\tau, \tau') &= \alpha_\ell p_{\ell 0}^k e^{p_{\ell 0}(\tau-\tau')} + \sum_{n=1}^m e^{p_{\ell n}(\tau-\tau')} r_{\ell n}^k \\ &\times \left[(\beta_{\ell n} \sin k\theta_{\ell n} + \gamma_{\ell n} \cos k\theta_{\ell n}) \cos q_{\ell n}(\tau-\tau') \right. \\ &\left. + (\beta_{\ell n} \cos k\theta_{\ell n} - \gamma_{\ell n} \sin k\theta_{\ell n}) \sin q_{\ell n}(\tau-\tau') \right] \quad (9) \end{aligned}$$

where

$$p_{\ell n} + iq_{\ell n} = r_{\ell n} e^{i\theta_{\ell n}}$$

Taking the limit as τ approaches τ' from above,

$$\begin{aligned} \left. \frac{d^k H_\ell(\tau, \tau')}{d\tau^k} \right|_{\tau \rightarrow \tau'} &= \alpha_\ell p_{\ell 0}^k + \sum_{n=1}^m r_{\ell n}^k \left[\beta_{\ell n} \sin k\theta_{\ell n} + \gamma_{\ell n} \cos k\theta_{\ell n} \right] \\ &= \delta_{\ell k}, \quad k=0, 1, 2, \dots, \ell \quad (10) \end{aligned}$$

gives $\ell + 1$ linear equations in $\ell + 1$ unknowns, and the constants α_ℓ , $\beta_{\ell n}$, and $\gamma_{\ell n}$ can be determined. These constants are given in App. A.

The Green's function can now be found, and the solution of Eq. 6 can be written

$$b_\ell(\tau) = \int_0^\tau G_\ell(\tau-\tau') B_\ell(\tau') d\tau' \quad (11)$$

In order to evaluate the right-hand side of Eqs. 1, 2, and 3, the first $\ell + 1$ derivatives of $b_\ell(\tau)$ are needed. By direct differentiation of Eq. 11 and application of the boundary condition on H_ℓ (and, hence on G_ℓ) expressed in Eq. 10, one can write

$$\frac{d^k b_\ell}{d\tau^k} = R^{\ell+2} \left[\delta_{k, \ell+1} B_\ell(\tau) + \int_0^\tau H_\ell^{(k)}(\tau, \tau') B_\ell(\tau') d\tau' \right] \quad (12)$$

$k=0, 1, 2, \dots, \ell+1$

where

$$H_\ell^{(k)}(\tau, \tau') = \frac{\partial^k}{\partial \tau^k} H_\ell(\tau, \tau')$$

For simplicity of notation, let

$$C_\ell^k(\tau) = \int_0^\tau H_\ell^{(k)}(\tau, \tau') B_\ell(\tau') d\tau' \quad (13)$$

Substituting the right-hand side of Eq. 9 for $H_\ell^{(k)}(\tau, \tau')$ and defining the symbols $I_{x\ell}(\tau)$, $I_{c\ell n}(\tau)$, and $I_{s\ell n}(\tau)$ for the following integrals:

$$I_{x\ell}(\tau) = \int_0^\tau e^{p_{\ell 0}(\tau-\tau')} B_\ell(\tau') d\tau' \quad (14)$$

$$I_{c\ell n}(\tau) = \int_0^\tau e^{p_{\ell n}(\tau-\tau')} \cos q_{\ell n}(\tau-\tau') B_\ell(\tau') d\tau' \quad (15)$$

$$I_{s\ell n}(\tau) = \int_0^\tau e^{p_{\ell n}(\tau-\tau')} \sin q_{\ell n}(\tau-\tau') B_\ell(\tau') d\tau' \quad (16)$$

$n=1, 2, \dots, m$

one can write $C_\ell^k(\tau)$ as

$$C_\ell^k(\tau) = \alpha_\ell p_{\ell 0}^k I_{x\ell}(\tau) + \sum_{n=1}^m r_{\ell n}^k \left[(\beta_{\ell n} \sin k\theta_{\ell n} + \gamma_{\ell n} \cos k\theta_{\ell n}) I_{c\ell n}(\tau) \right. \\ \left. + (\beta_{\ell n} \cos k\theta_{\ell n} - \gamma_{\ell n} \sin k\theta_{\ell n}) I_{s\ell n}(\tau) \right] \quad (17)$$

The terms in the expansion of E_r , Eq. 1, can be written as

$$\frac{1}{r} \bar{H}_\ell(r) a_\ell(t^*) = \sum_{j=0}^{\ell} \mu_{\ell j} \left(\frac{R}{r} \right)^{j+2} C_\ell^{(\ell-j)}(\tau) \quad (18)$$

Similarly, terms in the expansion of E_θ , Eq. 2, can be written as

$$\Lambda_\ell(r) a_\ell(t^*) = \frac{R}{r} B_\ell(\tau) + \sum_{j=0}^{\ell+1} \nu_{\ell j} \left(\frac{R}{r} \right)^{j+1} C_\ell^{(\ell+1-j)}(\tau) \quad (19)$$

The terms in the expansion of B_ϕ are

$$\frac{1}{c} \frac{\partial}{\partial t^*} \bar{H}_\ell(r) a_\ell(t^*) = \frac{R}{r} B_\ell(\tau) + \sum_{j=0}^{\ell} \mu_{\ell j} \left(\frac{R}{r} \right)^{j+1} C_\ell^{(\ell+1-j)}(\tau) \quad (20)$$

Finally, Eqs. 1, 2, and 3 can be written using Eqs. 18, 19, and 20 as

$$E_r = - \sum_{\ell=1}^{\infty} \sqrt{\ell(\ell+1)} \sum_{j=0}^{\ell} \mu_{\ell j} \left(\frac{R}{r} \right)^{j+2} C_\ell^{\ell-j}(\tau) \bar{P}_\ell(\cos \theta) \quad (21)$$

$$E_{\theta} = \sum_{\ell=1}^{\infty} \left[\frac{R}{r} B_{\ell}(\tau) + \sum_{j=0}^{\ell+1} \nu_{\ell j} \left(\frac{R}{r} \right)^{j+1} C_{\ell}^{\ell+1-j}(\tau) \right] \bar{P}_{\ell}^1(\cos \theta) \quad (22)$$

$$B_{\phi} = \sum_{\ell=1}^{\infty} \left[\frac{R}{r} B_{\ell}(\tau) + \sum_{j=0}^{\ell} \mu_{\ell j} \left(\frac{R}{r} \right)^{j+1} C_{\ell}^{\ell+1-j}(\tau) \right] \bar{P}_{\ell}^1(\cos \theta) \quad (23)$$

Given the coefficients of an expansion of E_{θ} at $r = R$, $B_{\ell}(\tau)$, one first calculates the convolution integrals $I_{x\ell}(\tau)$, $I_{c\ell n}(\tau)$, and $I_{s\ell n}(\tau)$, Eqs. 14, 15, and 16, for each value of τ . The values of $C_{\ell}^k(\tau)$ are found for the same τ values from Eq. 17. The fields E_r , E_{θ} , and B_{ϕ} can then be determined at any value of r and a time history can be calculated using Eqs. 21, 22, and 23.

III. THE NUMERICAL INTEGRATION

In performing the numerical integration indicated in Eqs. 14, 15, and 16, one need not integrate from the origin for each new τ value chosen. In evaluating $I_{x\ell}(\tau+\Delta\tau)$, $I_{c\ell n}(\tau+\Delta\tau)$, and $I_{s\ell n}(\tau+\Delta\tau)$, the properties of the exponential and trigonometric functions can be used to evaluate the integral from zero to τ using $I_{x\ell}(\tau)$, $I_{c\ell n}(\tau)$, and $I_{s\ell n}(\tau)$. Thus $I_{x\ell}(\tau+\Delta\tau)$ can be written

$$I_{x\ell}(\tau+\Delta\tau) = e^{p_{\ell 0}\Delta\tau} I_{x\ell}(\tau) + \int_{\tau}^{\tau+\Delta\tau} e^{p_{\ell 0}(\tau+\Delta\tau-\tau')} B_{\ell}(\tau') d\tau' \quad (24)$$

Applying the trapezoidal rule to the above integral, one obtains

$$I_{x\ell}(\tau+\Delta\tau) = e^{p_{\ell 0}\Delta\tau} \left[I_{x\ell}(\tau) + \frac{\Delta\tau}{2} B_{\ell}(\tau) \right] + \frac{\Delta\tau}{2} B_{\ell}(\tau+\Delta\tau) \quad (25)$$

The trapezoidal rule will probably work well in most cases. However, it may happen that even though the data points are close enough together to describe B_{ℓ} very well, they may be far apart with regard to the behavior of the kernel of the integral (in this case an exponential, in the other cases, the product of an exponential and a trigonometric function). In this event it is assumed that $B_{\ell}(\tau)$ follows a straight line over the interval $(\tau, \tau+\Delta\tau)$, since the data are chosen to accurately describe $B_{\ell}(\tau)$. The integral is then evaluated exactly. Thus, for large $\Delta\tau$ let

$$B_{\ell}(\tau') = C\tau' + D \quad (26)$$

$$C = \frac{B_{\ell}(\tau + \Delta\tau) - B_{\ell}(\tau)}{\Delta\tau}$$

$$D = B_{\ell}(\tau) - C\tau$$

The integral in Eq. 24 can be evaluated exactly, resulting in

$$I_{x\ell}(\tau + \Delta\tau) = e^{p_{\ell 0} \Delta\tau} I_{x\ell}(\tau) - \frac{1}{p_{\ell 0}} \left[\left(1 - e^{p_{\ell 0} \Delta\tau} \right) \left(B_{\ell}(\tau) + \frac{C}{p_{\ell 0}} \right) + B_{\ell}(\tau + \Delta\tau) - B_{\ell}(\tau) \right] \quad (27)$$

Similarly, for $I_{c\ell n}(\tau + \Delta\tau)$ the integral is split as follows:

$$I_{c\ell n}(\tau + \Delta\tau) = e^{p_{\ell n} \Delta\tau} \left[I_{c\ell n}(\tau) \cos q_{\ell n} \Delta\tau - I_{s\ell n}(\tau) \sin q_{\ell n} \Delta\tau \right] + \int_{\tau}^{\tau + \Delta\tau} e^{p_{\ell n}(\tau + \Delta\tau - \tau')} \cos q_{\ell n}(\tau + \Delta\tau - \tau') B_{\ell}(\tau') d\tau' \quad (28)$$

For $\Delta\tau$ small, the trapezoidal rule is used:

$$I_{c\ell n}(\tau + \Delta\tau) = e^{p_{\ell n} \Delta\tau} \left[\left(I_{c\ell n}(\tau) + \frac{\Delta\tau}{2} B_{\ell}(\tau) \right) \cos q_{\ell n} \Delta\tau - I_{s\ell n}(\tau) \sin q_{\ell n} \Delta\tau \right] + \frac{\Delta\tau}{2} B_{\ell}(\tau + \Delta\tau) \quad (29)$$

When $\Delta\tau$ is large, Eq. 26 is used for $B_{\ell}(\tau')$ and the integral in Eq. 28 can be evaluated exactly:

$$\begin{aligned}
I_{c\ell n}(\tau+\Delta\tau) = & e^{p_{\ell n}\Delta\tau} \left[I_{c\ell n}(\tau) \cos q_{\ell n}\Delta\tau - I_{s\ell n}(\tau) \sin q_{\ell n}\Delta\tau \right] \\
& - \frac{1}{r_{\ell n}^2} \left[\left(1 - e^{p_{\ell n}\Delta\tau} \cos q_{\ell n}\Delta\tau \right) \left(p_{\ell n} B_{\ell}(\tau) \right. \right. \\
& \left. \left. + \frac{C}{r_{\ell n}^2} (p_{\ell n}^2 - q_{\ell n}^2) \right) - e^{p_{\ell n}\Delta\tau} \sin q_{\ell n}\Delta\tau \left(q_{\ell n} B_{\ell}(\tau) \right. \right. \\
& \left. \left. + \frac{2Cp_{\ell n}q_{\ell n}}{r_{\ell n}^2} \right) + C\Delta\tau p_{\ell n} \right] \quad (30)
\end{aligned}$$

Similarly, when the trapezoidal rule is used to approximate $I_{s\ell n}(\tau+\Delta\tau)$ for small $\Delta\tau$, one obtains

$$\begin{aligned}
I_{s\ell n}(\tau+\Delta\tau) = & e^{p_{\ell n}\Delta\tau} \left[\left(I_{c\ell n}(\tau) + \frac{\Delta\tau}{2} B_{\ell}(\tau) \right) \sin q_{\ell n}\Delta\tau \right. \\
& \left. + I_{s\ell n}(\tau) \cos q_{\ell n}\Delta\tau \right] \quad (31)
\end{aligned}$$

For large $\Delta\tau$, again let $B_{\ell}(\tau) = C\tau + D$, and the integral $I_{s\ell n}(\tau+\Delta\tau)$ can be expressed as

$$\begin{aligned}
I_{s\ell n}(\tau+\Delta\tau) = & e^{p_{\ell n}\Delta\tau} \left[I_{c\ell n}(\tau) \sin q_{\ell n}\Delta\tau + I_{s\ell n}(\tau) \cos q_{\ell n}\Delta\tau \right] \\
& + \frac{1}{r_{\ell n}^2} \left[\left(1 - e^{p_{\ell n}\Delta\tau} \cos q_{\ell n}\Delta\tau \right) \left(q_{\ell n} B_{\ell}(\tau) + \frac{2Cp_{\ell n}q_{\ell n}}{r_{\ell n}^2} \right) \right. \\
& \left. + e^{p_{\ell n}\Delta\tau} \sin q_{\ell n}\Delta\tau \left(p_{\ell n} B_{\ell}(\tau) + \frac{C}{r_{\ell n}^2} (p_{\ell n}^2 - q_{\ell n}^2) \right) \right. \\
& \left. + C\Delta\tau q_{\ell n} \right] \quad (32)
\end{aligned}$$

The criterion used to determine whether $\Delta\tau$ is small or large depends upon the polynomial roots and $\Delta\tau$. At this time, if $p_{\ell 0} \Delta\tau < .1$ then $\Delta\tau$ is considered small, and the trapezoidal method is used for the evaluation of $I_{x\ell}(\tau + \Delta\tau)$ by Eq. 25. If $r_{\ell n} \Delta\tau < .1$, then $\Delta\tau$ is again considered small, and the trapezoidal method is used to integrate $I_{s\ell n}(\tau + \Delta\tau)$ and $I_{c\ell n}(\tau + \Delta\tau)$ by Eqs. 29 and 31. Otherwise, the other method is used.

Since the roots and coefficients appearing in the function H_{ℓ} are not dependent on any physical parameters in the problem, they are mathematical constants and once determined can be used over and over for any values of the physical parameters.

IV. DESCRIPTION OF PROGRAM M

Program M has been developed to extrapolate transient multipole fields through a computerized system according to the method explained in Secs. I through III.

The program requires 165 K octal locations on the CDC 6600. Four tapes labeled 1, 2, 4, and 8 are needed. Tape 2 is the input tape, while Tape 1 contains the coefficients of the normalized Legendre polynomials that were picked from the input tape. Tape 4 contains the calculated quantities referred to as $C_{\ell}^k(\tau)$. Tape 8 enables the operator to dump and restart the program periodically. Tape 8 is a half-inch tape with 556 bits per inch. If the number of time points is less than 2000, then Tapes 1 and 4 can be half-inch tapes; otherwise, they must be one-inch tapes with 800 bits per inch.

The central processor (CP) time can be approximated as follows:

(number of time points) x (.6 sec) = time taken to calculate
all the $C_{\ell}^k(\tau)$;

(number of time points) x (.04 sec) = time to extrapolate.

The peripheral processor (PP) time is approximately twice the CP time. These times should always overestimate the time required. The program is set up to dump itself on Tape 8 every 15 minutes. The ability to restart after dumping is included only in the portion of the program that calculates the quantities $C_{\ell}^k(\tau)$. The extrapolation procedure takes so little time that there is no need for a restart capability during that section.

INPUT

The tape input consists of the coefficients of the Legendre expansion of E_θ , E_ϕ , and E_r (given on Tape 2) in blocks of 496 words, each terminated by an end-of-file mark, as shown below.

<u>Word</u>	<u>Description</u>
1	observer number (floating point)
2	time (retarded time in seconds)
3-22	coefficients of E_θ
23-42	coefficients of E_r
43-62	coefficients of E_ϕ
63-124	same as words 1-62
125-186	" " " "
187-248	" " " "
249-310	" " " "
311-372	" " " "
373-434	" " " "
435-496	" " " "

In addition, the origin observer number, the corresponding radius, the radii to which the extrapolations are performed, and the observer numbers and angles are input on cards.

<u>Cards</u>	<u>Columns</u>	<u>Format</u>	<u>Description</u>
1	1-10	I10	observer number of origin of extrapolation
	11-20	E10.3	radius, in meters, of origin
2, ..., n ⁴	1-10	I10	observer number of extrapolation
	11-20	E10.3	radius of extrapolation (meters)
	21-30	E10.3	angle of extrapolation (degrees)
last card	1-80		blank

The polynomial roots ($p_{\ell n} \pm iq_{\ell n}$) and the Green's function coefficients ($\beta_{\ell n}, \gamma_{\ell n}$) are also on input cards and are read in prior to the above data. However, these cards are the same for each set of calculations and should remain with the source deck. It is important to remember that these cards, as well as data card 1, are not used with the restart program.

OUTPUT

All output is on microfilm. The message below is printed each time a restart group is dumped on Tape 8.

RESTART GROUP NO _____ IS COMPLETED

LAST TIME POINT WAS _____

Also, at that time, the extrapolated fields are printed and plotted. Samples of input and output are shown on the following pages.

⁴ These cards start the data cards necessary for the restart program.

RUN NUMBER 3400
(14976..90.)

<u>TIME</u>	<u>ERADIAL</u>	<u>ETHETA</u>	<u>BPIII</u>
0.	0.	0.	0.
1.0006882E-09	-1.7725442E-14	2.9561382E-02	9.8530588E-11
2.0013803E-09	-7.1332043E-14	6.3609247E-02	2.1200174E-10
3.0020725E-09	-1.5397828E-13	1.0242935E-01	3.4137125E-10
4.0027646E-09	-9.0513321E-14	1.4625592E-01	4.8751608E-10
5.0034568E-09	-3.4398399E-13	1.9557643E-01	6.5179472E-10
6.0041489E-09	-9.7588775E-13	2.5069481E-01	8.3519229E-10
7.0048411E-09	-1.1894905E-13	3.1124492E-01	1.0376415E-09
8.0055332E-09	-1.8109012E-12	3.7900290E-01	1.2624414E-09
9.0062254E-09	-1.2854060E-12	4.5252319E-01	1.5078824E-09
1.0006918E-08	-2.3706373E-12	5.3351856E-01	1.7773188E-09
1.1007610E-08	-4.7950199E-12	6.2225587E-01	2.0718328E-09
1.2008302E-09	-6.3652238E-12	7.1680717E-01	2.3864419E-09
1.3008994E-08	1.0760466E-12	8.1381586E-01	2.7137588E-09
1.4009686E-08	-7.1647338E-12	9.2329428E-01	3.0740753E-09
1.5010378E-08	-5.9038515E-12	1.0354243E+00	3.4488686E-09
1.6011070E-08	-8.8765915E-12	1.1556631E+00	3.8485119E-09
1.7011763E-08	-6.4697238E-12	1.2800036E+00	4.2642331E-09
1.8012455E-08	-2.6925373E-12	1.4101130E+00	4.6998756E-09
1.9013147E-08	-5.6939536E-12	1.5496928E+00	5.1640664E-09
2.0013839E-08	-1.6413419E-11	1.6981895E+00	5.6520619E-09
2.1014531E-08	-1.9204368E-11	1.8508751E+00	6.1619452E-09
2.2015223E-08	-6.5922642E-12	2.0033696E+00	6.6775986E-09
2.3015915E-08	-3.1971062E-11	2.1764884E+00	7.2390666E-09
2.4016608E-08	-3.4421143E-11	2.3473180E+00	7.8081792E-09
2.5017300E-08	-4.5600619E-11	2.5279938E+00	8.4037093E-09
2.6017992E-08	-4.8167243E-12	2.6955284E+00	8.9881683E-09
2.7018684E-08	-1.1549070E-11	2.8870553E+00	9.6211620E-09
2.8019376E-08	-9.0344092E-12	3.0813344E+00	1.0271537E-08
2.9020068E-08	7.9075706E-12	3.2774247E+00	1.0937352E-08
3.0020760E-08	-7.8389277E-11	3.5185944E+00	1.1690663E-08
3.1021453E-08	-4.0504430E-11	3.7185576E+00	1.2381371E-08
3.2022145E-08	-2.1364277E-11	3.9310209E+00	1.3096350E-08
3.3022837E-08	-1.0194083E-10	4.1884246E+00	1.3909864E-08
3.4023529E-08	-8.5429840E-11	4.4164974E+00	1.4684533E-08
3.5024221E-08	-3.7698652E-11	4.6377855E+00	1.5445393E-08
3.6024913E-08	-4.0273819E-11	4.8852286E+00	1.6270821E-08
3.7025605E-08	-5.1281697E-11	5.1417310E+00	1.7117980E-08
3.8026298E-08	-9.7854093E-11	5.4205628E+00	1.8024903E-08
3.9026990E-08	-6.6648639E-11	5.6708952E+00	1.8874563E-08

Fig. 1--Sample Output

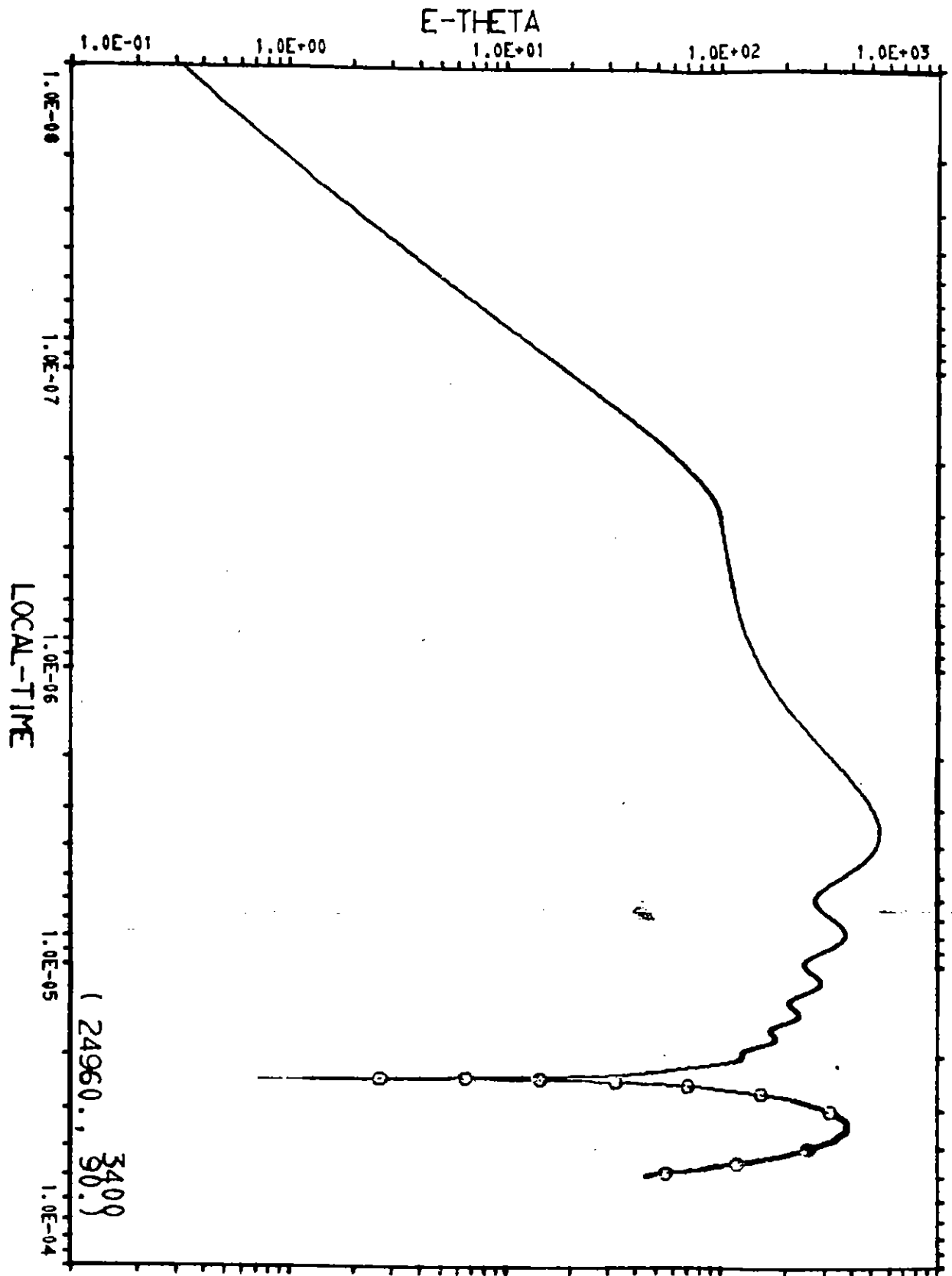


Fig. 2-- E_{θ} Graph (Log-log)

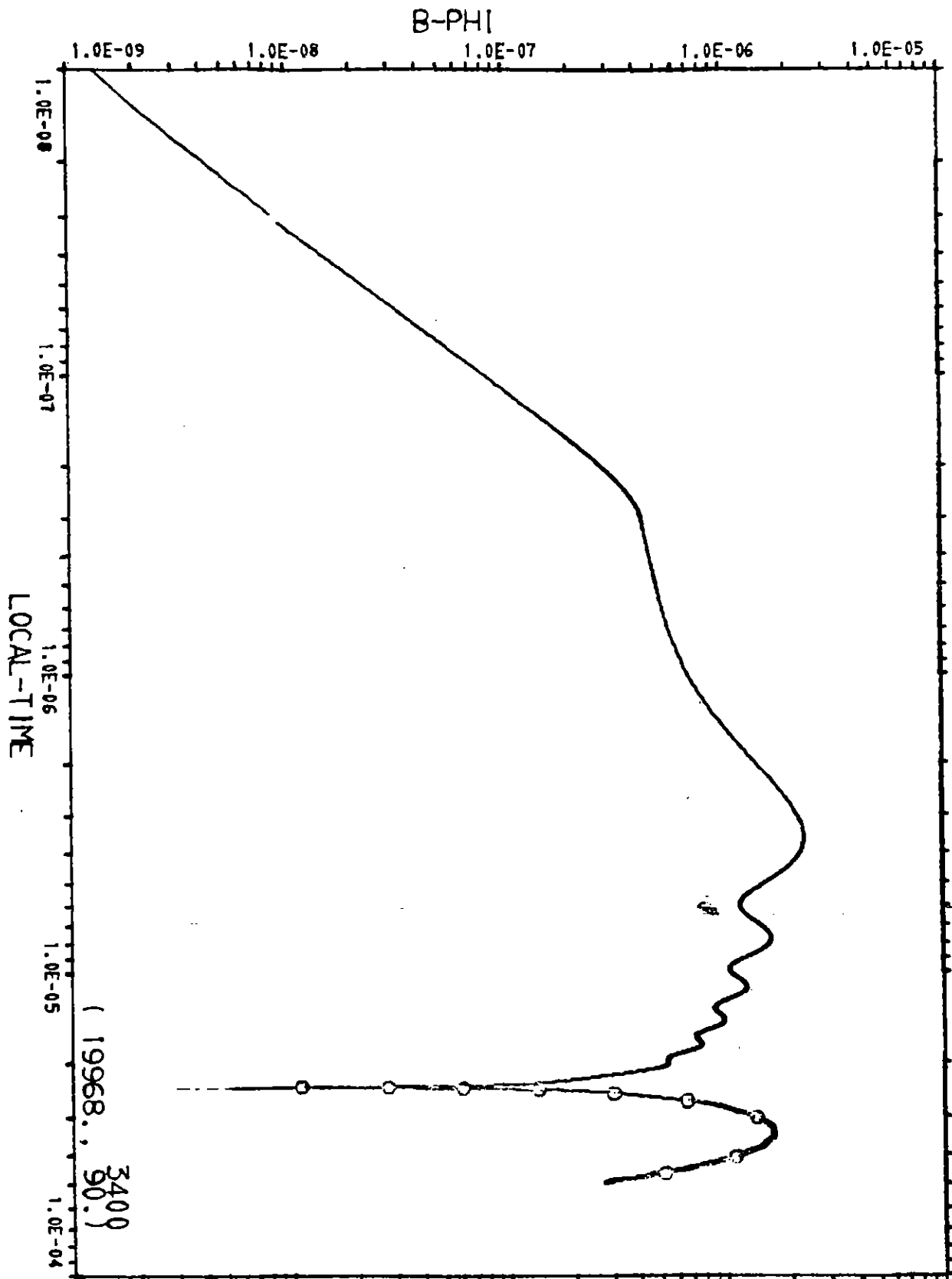


Fig. 3-- B_{ϕ} Graph (Log-log)

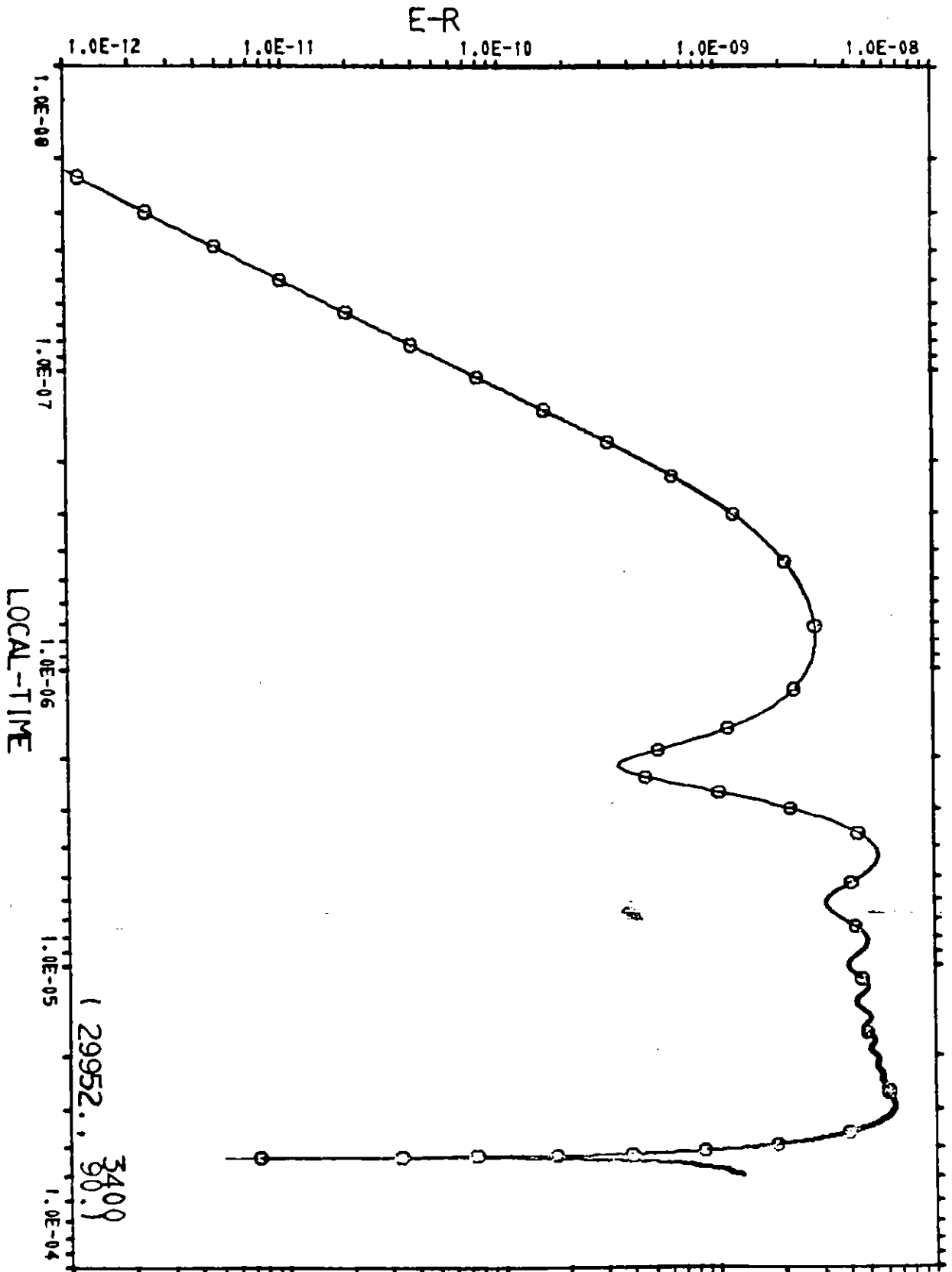


Fig. 4-- E_r Graph (Log-log)

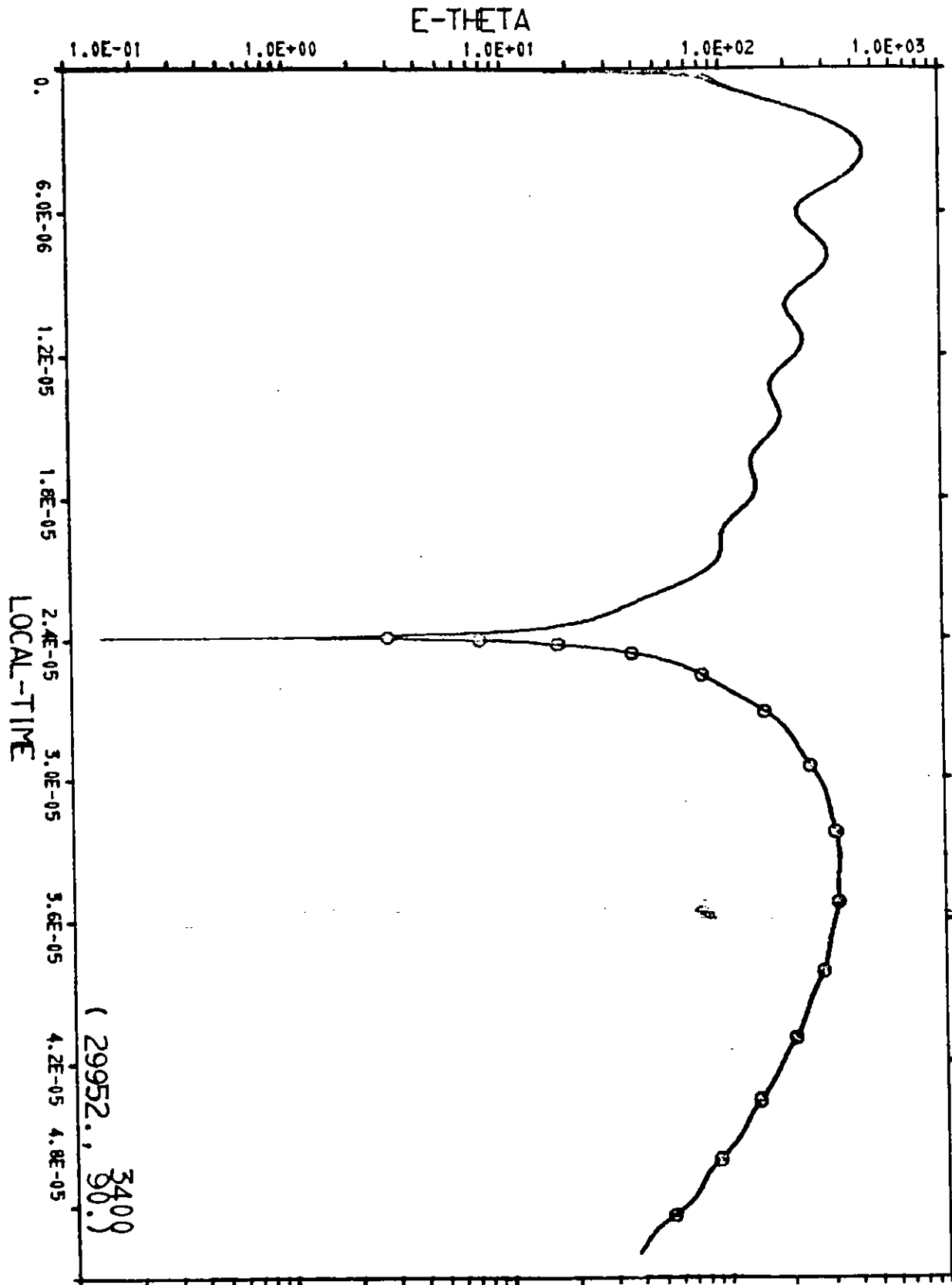
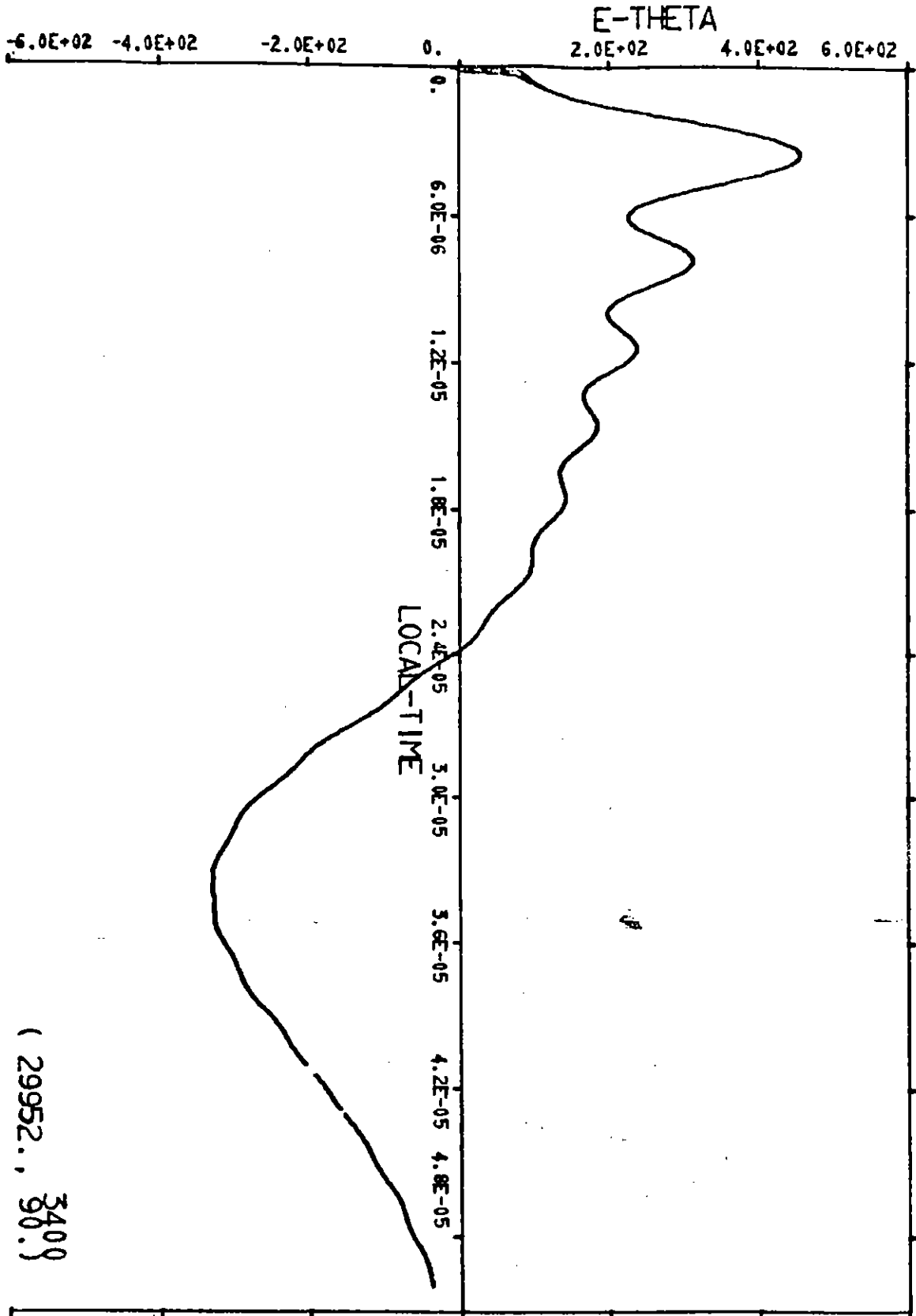


Fig. 5-- E_{θ} Graph (Log-linear)



(29952., 3409)

Fig. 6--E_θ Graph (Linear-linear)

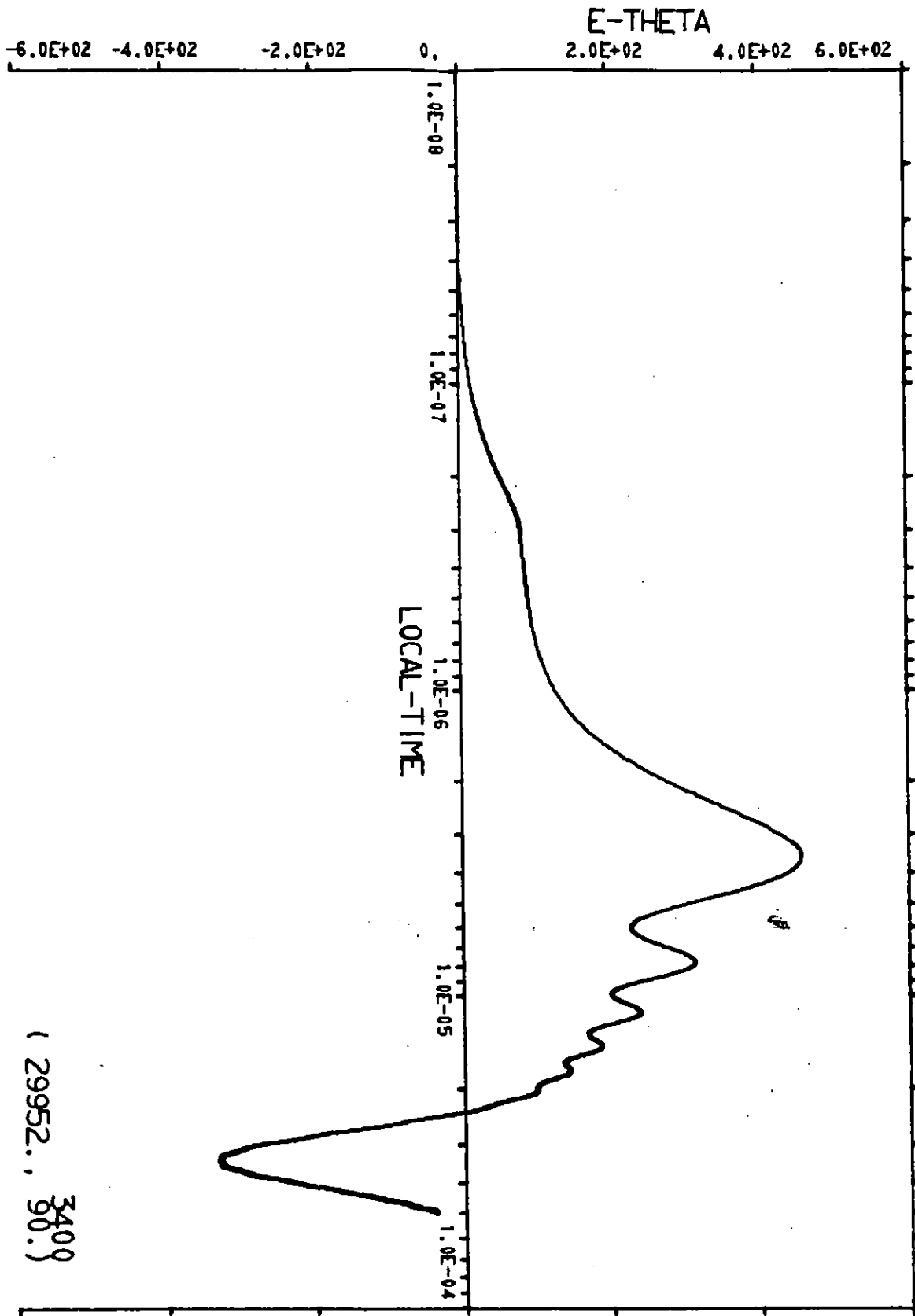


Fig. 7--E Graph (Linear-log)

APPENDIX A

GREEN'S FUNCTION COEFFICIENTS
(COMPUTER LISTING)

GREENS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
1		1.154700538E+00	0.
2	2.459477531E-01	1.216726137E-01 2.459477531E-01	-2.459477531E-01 0.
3		1.250481260E-01 -2.357121774E-02	3.336973334E-02 -3.336973334E-02
4	1.750733791E-02	1.264723817E-02 -4.381193554E-03	-1.795235275E-02 4.450148329E-04
5		5.854831311E-03 -1.422342446E-03 -1.522683925E-04	1.955108009E-03 -2.293544435E-03 3.384364262E-04
6	5.610986921E-04	5.032619124E-04 -2.559632734E-04 1.483961877E-05	-6.136818310E-04 3.167221423E-05 2.091092460E-05
7		1.396937552E-04 -3.745467255E-05 -6.489338731E-06 1.495148318E-06	5.137458704E-05 -7.025416450E-05 1.900164063E-05 -1.220631667E-07
8	1.014423883E-05	1.027253811E-05 -6.496285499E-06 9.203881178E-07 3.362813415E-08	-1.149788654E-05 4.820788491E-07 9.397943057E-07 -6.822543642E-08
9		2.011344840E-06 -5.617771988E-07 -1.572020373E-07 7.100580499E-08 -1.837343304E-09	7.809576674E-07 -1.176465636E-06 4.201240051E-07 -2.175298317E-08 -2.863053277E-09
10	1.174971877E-07	1.285288278E-07 -9.275785790E-08 1.847942247E-08 6.911866394E-10 -1.360198879E-10	-1.361649484E-07 3.134787774E-09 1.914324475E-08 -3.613798074E-09 3.526160692E-12

GREENS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
11		1.935537968E-08 -5.508427439E-09 -2.167540414E-09 1.316976252E-09 -1.259618143E-10 -2.447876133E-12	7.782037385E-09 -1.252151805E-09 5.262871471E-09 -4.253537204E-10 -1.023060727E-10 4.268992532E-12
12	9.455415045E-10	1.090996795E-09 -8.608565013E-10 2.075000265E-10 9.661797697E-12 -5.961571389E-12 7.814045132E-14	-1.112377194E-09 2.569915833E-12 2.249641843E-10 -6.329009602E-11 2.449322988E-12 1.423628390E-13
13		1.332203948E-10 -3.824698667E-11 -1.930072471E-11 1.397421099E-11 -2.164655096E-12 -2.642040693E-14 4.921821812E-15	5.488253674E-11 -9.261737099E-11 4.339519566E-11 -4.338124900E-12 -1.553682975E-12 2.312121472E-13 2.343181201E-14
14	5.591806104E-12	6.709128913E-12 -5.646908368E-12 1.539699500E-12 9.444466211E-14 -8.973979921E-14 6.260333255E-15 7.792272016E-17	-6.650125906E-12 -1.177488958E-13 1.747979616E-12 -6.219893675E-13 4.570981278E-14 4.482946642E-15 -1.143097157E-16
15		6.882519198E-13 -1.983366404E-13 -1.208735098E-13 9.859865150E-14 -2.014073647E-14 -3.938868015E-17 2.128277876E-16	2.986767378E-13 -5.050411823E-13 2.558490667E-13 -2.881846973E-14 -1.404752564E-14 3.484394083E-15 -9.972202772E-17

GREENS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
		-1.475875121E-18	-3.298933076E-18
16	2.532249605E-14	3.130306067E-14	-3.036195305E-14
		-2.766911750E-14	-1.099317716E-15
		8.226601011E-15	9.732490644E-15
		6.554518440E-16	-4.058807770E-15
		-7.706312548E-16	4.186323765E-16
		9.760710785E-17	5.310861987E-17
		5.058570337E-19	-6.637533367E-18
		-8.749930853E-20	-1.162194363E-20
17		2.766960881E-15	1.176691097E-15
		-7.982457263E-16	-2.117556238E-15
		-5.640508052E-16	1.137921305E-15
		5.022401228E-16	-1.377007933E-16
		-1.233359933E-16	-8.629634139E-17
		8.184798724E-19	2.884178407E-17
		2.745034803E-18	-1.804119693E-18
		-1.458029221E-19	-9.826048277E-20
		-1.281460758E-21	1.566660576E-21
18	9.061513704E-17	1.146860834E-16	-1.093421916E-16
		-1.053458407E-16	-5.795706014E-17
		3.339753762E-17	4.095405168E-17
		3.338334137E-18	-1.917573825E-17
		-4.443057363E-18	2.453631919E-18
		7.937378860E-19	3.789795671E-19
		-7.842450010E-21	-9.013065951E-20
		-3.900685114E-21	1.924947921E-21
		1.420964995E-23	4.136166887E-23
19		8.902080304E-18	3.827386986E-18
		-2.567289781E-18	-7.045826507E-18
		-2.043579730E-18	3.965367883E-18
		1.946986463E-18	-5.015429409E-19
		-2.460800900E-19	-3.878592947E-19
		6.984869630E-21	1.583644725E-19
		1.991594317E-20	-1.506003481E-20

GREENS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
		-2.137597346E-21	-9.317465793E-22
		-6.377146399E-24	1.009846812E-22
		8.711115867E-25	1.984685752E-25
20	2.626713742E-19	3.388441064E-19	-3.185758675E-19
		-3.210520846E-19	-2.171310909E-20
		1.069424222E-19	1.352796693E-19
		1.295073245E-20	-6.922083957E-20
		-1.870136934E-20	1.020423371E-20
		4.207384067E-21	1.882710831E-21
		-1.094486476E-22	-6.530646114E-22
		-4.464702403E-23	3.457568078E-23
		1.849806260E-24	1.229342789E-24
		1.216713085E-26	-1.230807579E-26
21		2.3423051E-20	1.0160007E-20
		-6.7481639E-21	-1.9055984E-20
		-5.9230187E-21	1.1132139E-20
		5.9572332E-21	-1.4473264E-21
		-1.8487103E-21	-1.3380253E-21
		3.1012924E-23	6.3201861E-22
		9.7259075E-23	-7.8902799E-23
		-1.5689975E-23	-5.1784384E-24
		2.0009426E-25	1.2726940E-24
		4.1326785E-26	-2.0449082E-26
		-7.4387430E-29	-3.0974797E-28
22	6.2927690E-22	8.2463349E-22	-7.6640316E-22
		-8.0156692E-22	-6.2679358E-23
		2.7769934E-22	3.6088742E-22
		3.9535967E-23	-1.9815465E-22
		-6.0548529E-23	3.2932150E-23
		1.6109640E-23	6.9929579E-24
		-6.6384889E-25	-3.1296348E-24
		-2.8063795E-25	2.6873725E-25
		2.6149045E-26	9.5507194E-27
		6.1609512E-29	-9.0773922E-28
		-5.3088760E-30	-1.7681020E-30

GREENS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
23		5.0930867E-23 -1.4676576E-23 -1.3929387E-23 1.4669249E-23 -4.9390785E-24 9.7987070E-26 3.4545199E-25 -7.3571241E-26 2.3435406E-27 4.2517965E-28 -1.4059579E-29 -7.1108083E-32	2.2241778E-23 -4.2383854E-23 2.5551975E-23 -3.3965325E-24 -3.6316163E-24 1.9226551E-24 -2.9246964E-25 -1.9775494E-26 8.2206720E-27 -3.7159768E-28 -9.4004453E-30 5.9971371E-32
24	1.3314010E-24	1.7716307E-24 -1.7548774E-24 6.2204478E-25 1.0712720E-25 -1.6529793E-25 4.9361786E-26 -2.5235337E-27 -1.2720268E-27 1.8494371E-28 -2.0138213E-30 -2.9273460E-31 1.4551254E-34	-1.6231000E-24 -1.6115201E-25 8.3982214E-25 -4.8483543E-25 8.5947483E-26 2.2053054E-26 -1.1493455E-26 1.3223388E-27 4.6191497E-29 -1.1452644E-29 1.2767719E-31 1.5613068E-33
25		8.0421360E-26 -2.4085912E-26 -2.2489131E-26 2.5535734E-26 -9.5652898E-27 4.1296588E-28 7.7665402E-28 -2.1887878E-28 1.3711667E-29 1.7983372E-30 -1.7683279E-31	3.4874602E-26 -6.7781091E-26 4.2739134E-26 -6.5453013E-27 -6.5275031E-27 4.0119770E-27 -7.6459869E-28 -3.3869572E-29 2.9260769E-29 -2.5814010E-30 -3.3467438E-32

GRFNLS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
		2.4209175E-34	4.6242906E-33
		2.0343775E-35	5.5387262E-36
26	2.0780419E-27	2.7888654E-27	-2.5486191E-27
		-2.8216855E-27	-2.6442188E-28
		1.0383213E-27	1.4051110E-27
		1.8801048E-28	-8.5838111E-28
		-3.1506805E-28	1.6707534E-28
		1.0583406E-28	4.4865899E-29
		-7.2192198E-30	-2.7853745E-29
		-3.4861888E-30	4.1451423E-30
		7.2476444E-31	9.5246695E-32
		-2.3665123E-32	-6.1225321E-32
		-2.4863615E-33	2.3826213E-33
		6.6527081E-35	4.5057985E-35
		2.5966362E-37	-1.8752383E-37
27		5.2830400E-29	2.0403048E-29
		-2.1272595E-29	-4.2659276E-29
		-9.4599457E-30	3.2319552E-29
		1.7166902E-29	-9.9667505E-30
		-9.3702814E-30	-2.4106139E-30
		1.9066259E-30	3.3448310E-30
		3.7708844E-31	-1.1698772E-30
		-2.8398872E-31	1.1773219E-31
		5.0618082E-32	2.8867922E-32
		-6.5913894E-34	-7.9485023E-33
		-6.0162594E-34	4.1579149E-34
		3.3435882E-35	2.0962670E-35
		3.3098079E-37	-8.9641428E-37
		-2.9675447E-39	-2.7182993E-39
28	2.9180249E-30	3.8981702E-30	-3.6565422E-30
		-4.0917065E-30	-2.7458589E-31
		1.6463323E-30	2.0479444E-30
		2.2169287E-31	-1.3803127E-30
		-5.1828091E-31	3.2611637E-31
		2.0800595E-31	6.5794238E-32

GREENS FUNCTION COEFFICIENTS

ORDER	ALPHA	BETA	GAMMA
		-2.2648532E-32	-5.7899222E-32
		-7.2291111E-33	1.1808777E-32
		2.3276008E-33	-1.3786837E-34
		-1.6296881E-34	-2.3122671E-34
		-1.0525636E-35	2.0361196E-35
		1.0807367E-36	1.1988876E-37
		-1.3028324E-39	-2.2863136E-38
		-7.4893804E-41	-2.9813439E-41
29		7.5753441E-33	-1.3395731E-33
		-1.2042670E-32	-1.8221419E-33
		9.1326069E-33	9.9409797E-33
		3.6425968E-34	-1.1038637E-32
		-5.2755589E-33	4.5978810E-33
		3.4644725E-33	4.7050294E-34
		-7.2824744E-34	-1.1726077E-33
		-1.4827622E-34	4.0046755E-34
		9.7979848E-35	-2.7146691E-35
		-1.3602044E-35	-1.1921527E-35
		-4.4686338E-37	2.2519684E-36
		1.8708971E-37	-4.7710591E-38
		-5.1662968E-39	-7.9036241E-39
		-1.5523285E-40	1.3210138E-40
		1.5954713E-43	7.1611665E-43
30	-4.6562108E-34	-7.8419428E-34	4.1170547E-34
		6.3076686E-34	4.1172939E-34
		1.8752187E-35	-5.5832686E-34
		-3.0208323E-34	1.8202266E-34
		1.6895392E-34	7.7947019E-35
		-1.3894387E-35	-7.9604181E-35
		-2.0312298E-35	1.9931698E-35
		7.8172020E-36	1.6149770E-36
		-6.2171894E-37	-1.6266746E-36
		-1.7775071E-37	2.2386559E-37
		3.3046735E-38	6.2132525E-39
		-5.9228805E-40	-2.5587219E-39
		-1.0292373E-40	6.0303407E-41

GREENS FUNCTION COEFFICIENTS

ORDER

ALPHA

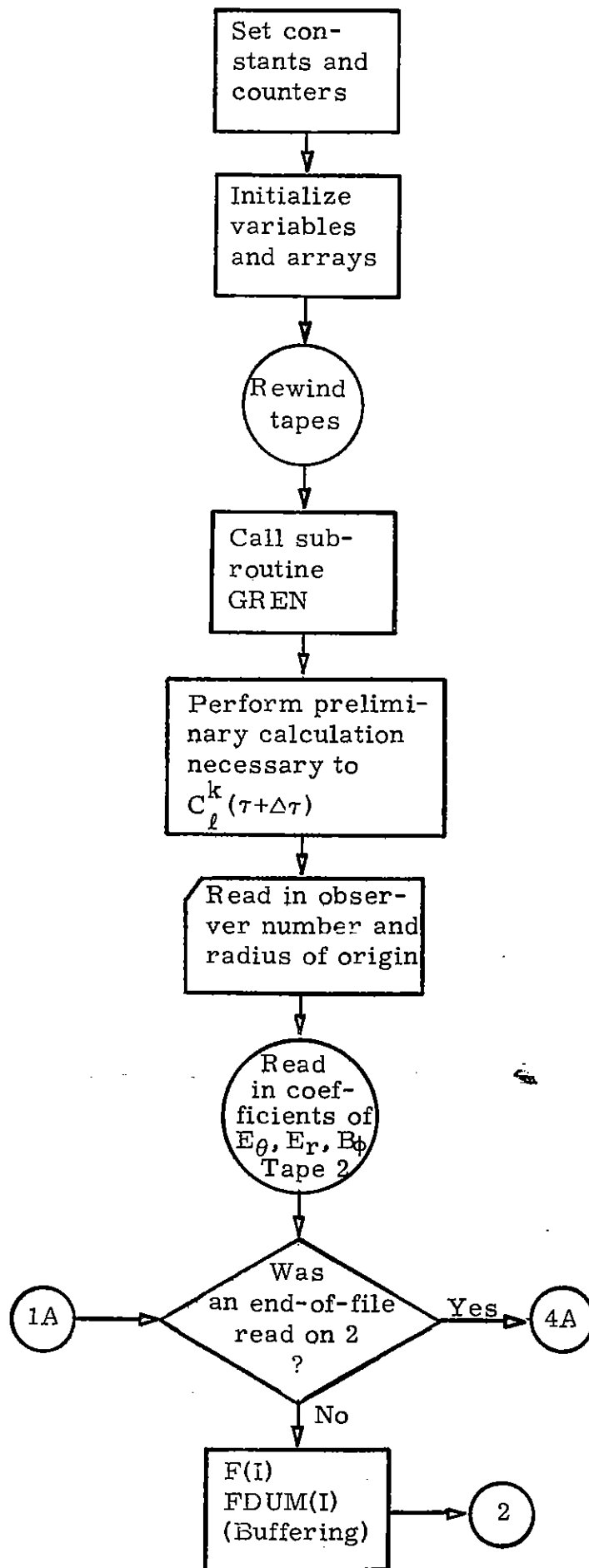
BETA

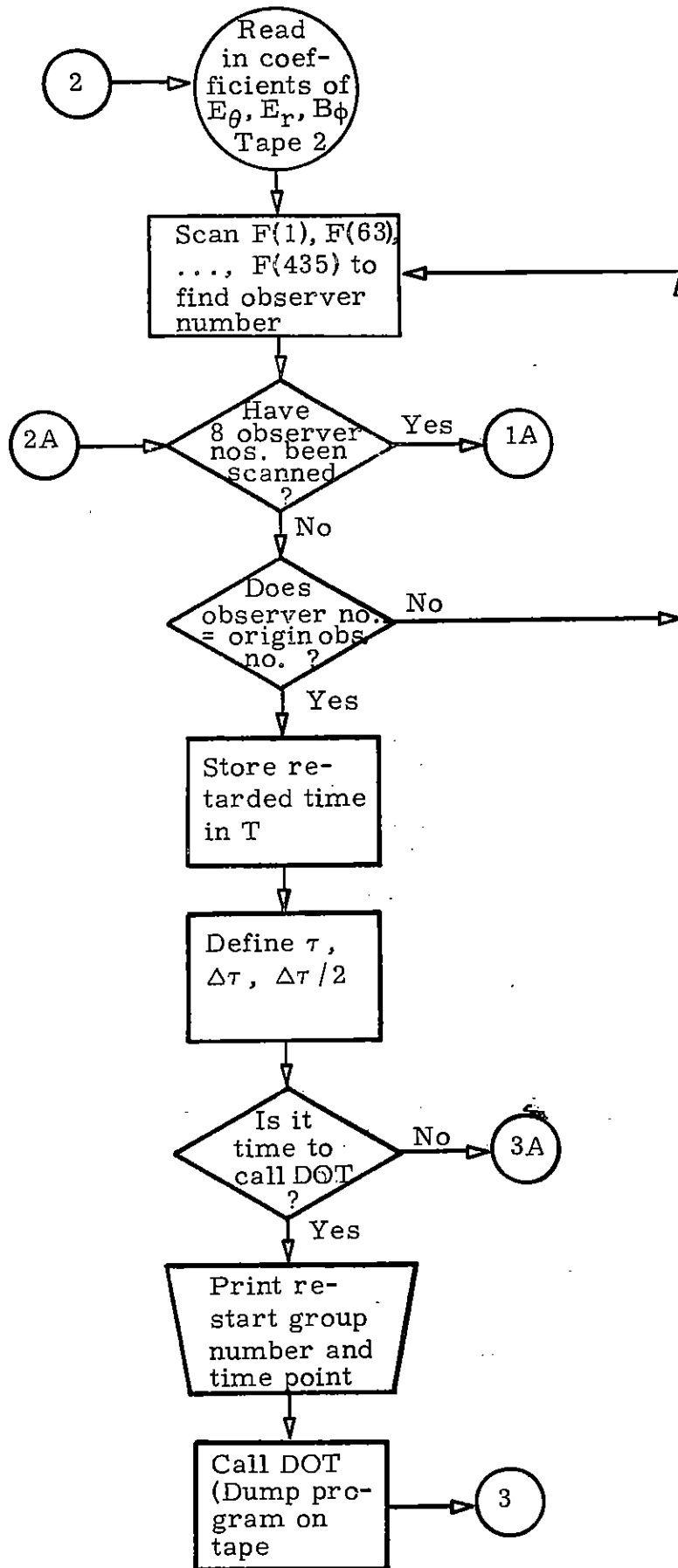
GAMMA

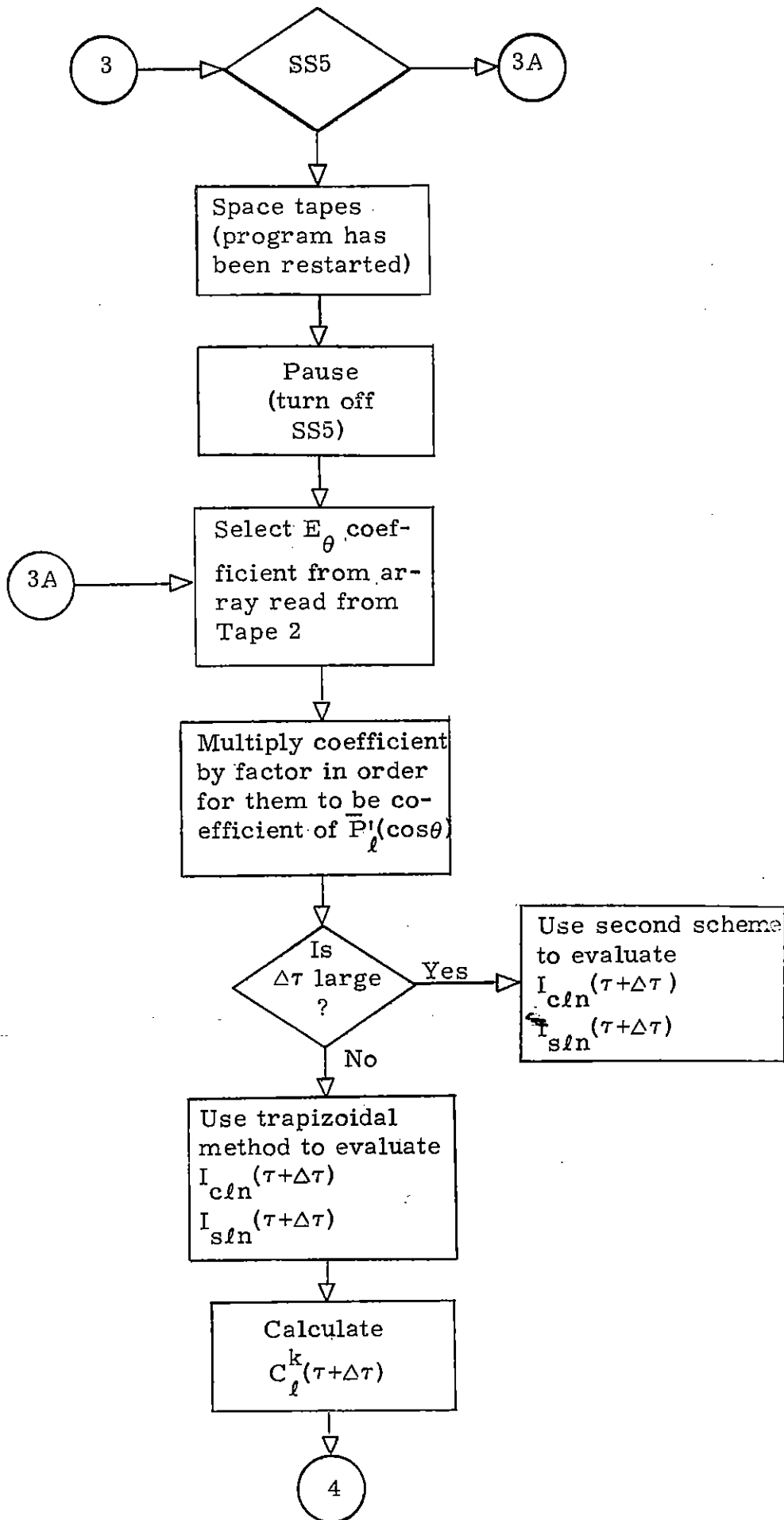
1.4137792E-42
7.7403594E-45

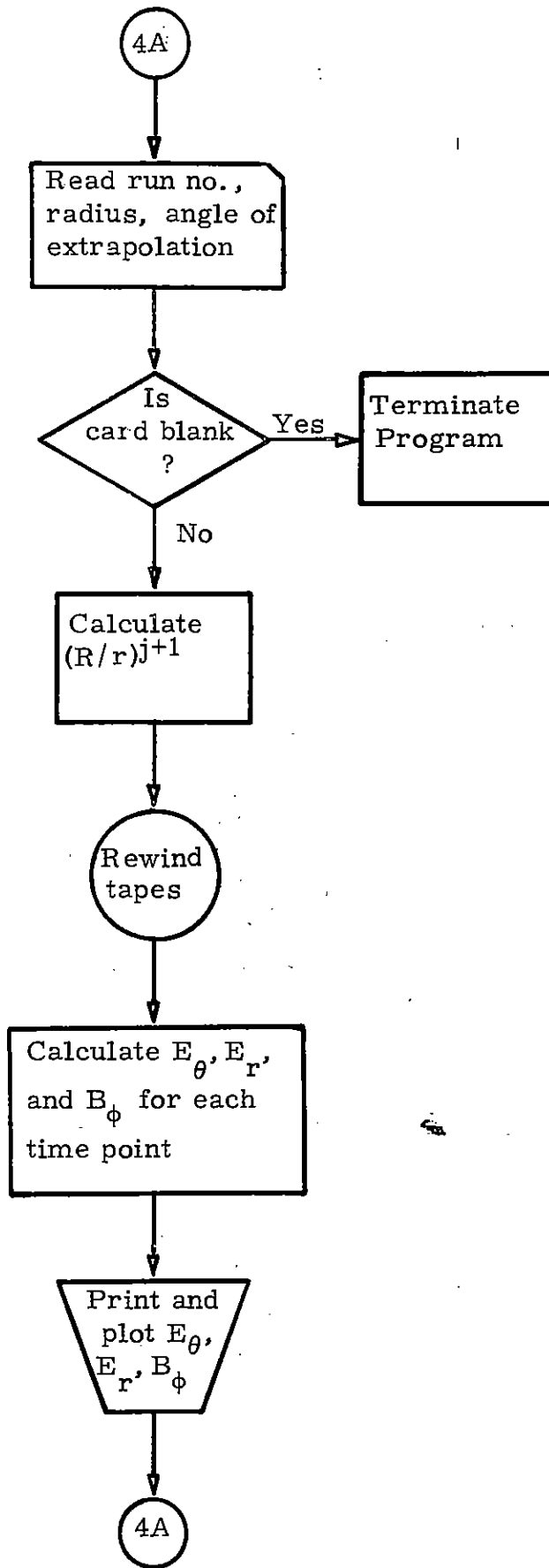
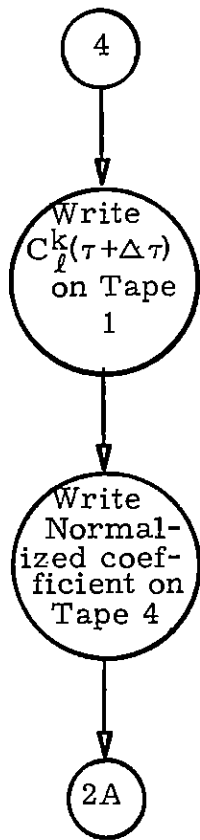
1.9189850E-42
-1.0538474E-45

APPENDIX B
FLOW CHARTS FOR PROGRAM M

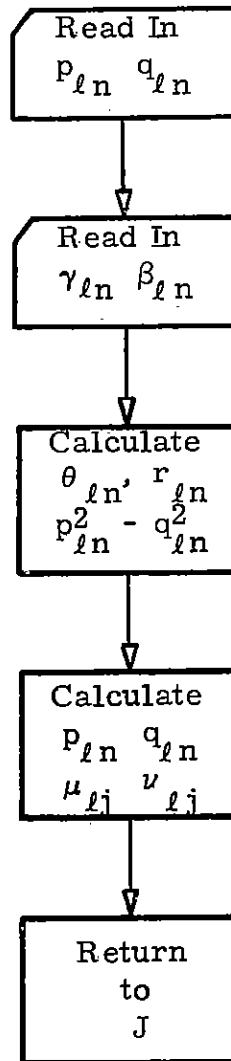




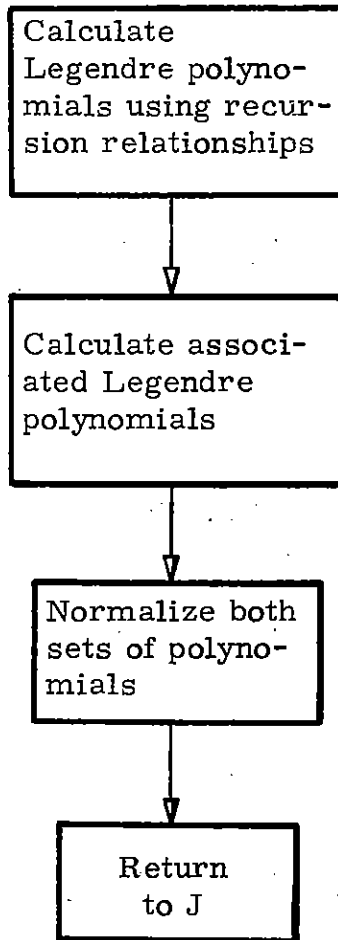




Subroutine GREN



Subroutine LEG



APPENDIX C
GLOSSARY FOR PROGRAM M

<u>Variable</u>	<u>Description</u>
ANG	angle, in degrees, of the extrapolated fields
B	E_{θ} coefficients of normalized Legendre polynomials, $B_{\ell}(\tau+\Delta\tau)$
BETA	$\beta_{\ell m}$
BLAST	$B_{\ell}(\tau)$
CEN	$I_{c\ell n}(\tau+\Delta\tau)$
CK	$C_{\ell}^k(\tau+\Delta\tau)$
DEL	$\Delta\tau / 2$
DT	$\Delta\tau$
E	E_{θ} field values
ER	E_r field values
EB	B_{ϕ} field values
F	input coefficient array
GAMMA	$\gamma_{\ell n}$
LIMIT	number of time points, including time=0
LLL	number of Legendre polynomials used
NOBS	observer number of origin of extrapolation
NNJ	run number of extrapolated fields
P	$p_{\ell n}$
PI	π
PCEN	$I_{c\ell n}(\tau)$
PMQ	$p_{\ell n}^2 - q_{\ell n}^2$
PN	\bar{P}_{ℓ}

<u>Variable</u>	<u>Description</u>
PQ	$p_{ln} q_{ln}$
P1	\bar{P}_l^{-1}
Q	q_{ln}
R	radius of origin of extrapolation
RDUN	1, if radiation term is to be plotted; 0, otherwise
ROC	radius (R)/speed of light
ROR	(radius of origin/radius of extrapolation) ^{j+1}
RL	radius of extrapolation (r)
RR	$(p_{ln}^2 + q_{ln}^2)^{1/2} = r_{ln}$
SEN	$I_{sln}(\tau + \Delta\tau)$
SM	criterion for determining which integration scheme to use
SUM1, SUMR	partial sums for E_r
SUM2, SUME	partial sums for E_θ
SUME3, SUMB	partial sums for B_ϕ
T	retarded time in seconds
TAU	dimensionless time (τ)
THE	$\pi - \sin^{-1}(q_{ln}/r_{ln}) = \theta_{ln}$
THETA	ANG expressed in radians
U	μ_{lj}
V	γ_{lj}
XT, XDOT	time increments for restarting

APPENDIX D
LISTING FOR PROGRAM M

```

PROGRAM M(INPUT,FILMPR,OUTPUT=FILMPR,TAPE1,TAPE2,TAPE4,TAPE8,FILMPJ 1
1L) J 2
DIMENSION GEN(220), SEN(220), PCEN(220), PN(45), P1(45), P(220), QJ 3
1(220), BETA(220), GAMMA(220), F(496), CK(450), R(20), H_LAST(20), TJ 4
2(5000), THE(220), RH(220), U(500), V(500), ROR(45), E(5000), ER(50J 5
300), =R(5000), PW(220), PMQ(220) J 6
DIMENSION XC(6000), XS(6000), RK(6000), ZZ(20) J 7
DOUBLE PRECISION TH,XSIN,XCOS,SUM,SUME,SUMR,SUMR,SUM1,SUM2,SUM3,PNJ 8
1,P1 J 9
DIMENSION FNUM(496), CKDM(450), BDUM(20) J 10
DOUBLE PRECISION ROR,RZ J 11
C SET CONSTANTS AND COUNTERS J 12
PI=3.141592653589793 J 13
C=300000000. J 14
LLL=20 J 15
SM=.1
XT=900.
XDOT=900.
IRCF=0 J 18
IRCC=0 J 19
ISTRT=0 J 20
PG=1. J 21
C INITIALIZE VARIABLES AND ARRAYS J 22
T(1)=0. J 23
TPR=0. J 24
F(1)=0. J 25
ER(1)=0. J 26
E=1)=0. J 27
DO 10 I=1,220 J 28
GEN(I)=0. J 29
10 SEN(I)=0. J 30
DO 20 I=1,20 J 31
20 H_LAST(I)=0. J 32
C REWIND TAPES J 33
REWIND 1 J 34
REWIND 2 J 35
REWIND 4 J 36
REWIND 8 J 37
C PERFORM PRELIMINARY CALCULATIONS NECESSARY TO C J 38
CALL GREN(P,Q,BETA,GAMMA,PMQ,RR,THE,PQ,U,V) J 39
IN=1 J 40
KN=0 J 41
KP=0 J 42
DO 50 I=1,LLL J 43
L=I*2-1 J 44
LMT=L+2 J 45
X=L J 46
ZZ(1)=SQRT(X*(X+1.)) J 47
DO 40 K=1,LMT J 48
XK=X-1 J 49
DO 30 N=1,I J 50
TH=THE(KP+N)*XK J 51
XCOS=DCOS(TH) J 52
XSIN=DSIN(TH) J 53
RZ=RR(KP+N)**(K-1) J 54
KN=*N+1 J 55
XC(*N)=XCOS J 56
XS(*N)=XSIN J 57
RK(*N)=RZ J 58
30 CONTINUE J 59
40 CONTINUE J 60

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	KP=KP+1	J	61
50	CONTINUE	J	62
C	READ IN OBSERVER NUMBER AND RADIUS OF ORGIN	J	63
	READ 400, NORBS,R,RDUM	J	64
	RDC=R/C	J	65
C	READ IN COEFF OF ETHETA,ERADIAL,BPHI FROM TAPE 2	J	66
	READ (2) FDUM	J	67
C	THIS IS POINT 1A	J	68
60	CONTINUE	J	69
C	WAS AN END-OF-FILE READ ON TAPE 2	J	70
C	IF YES GO TO 250 (4A) IF NO CONTINUE WITH 70		
	IF (EOF,2) 250,70		
70	CONTINUE	J	73
C	BUFFER IN THE INPUT COEFFICIENTS	J	74
	DO 40 I=1,496	J	75
80	F(I)=FDUM(I)	J	76
C	THIS IS POINT 2	J	77
C	READ IN COEFFICIENTS OF ETHETA,ERADIAL,BPHI FROM TAPE 2	J	78
	READ (2) FDUM	J	79
	IRCF=IRCF+1	J	80
C	SCAN F(1),F(63),...,F(435) TO FIND OBSERVER NO.	J	81
	DO 240 II=1,8		
	J=62*(II-1)+1		
	V=F(J)		
C	DOES OBSERVER NO. EQUAL ORGIN ORSERVER NO.	J	85
C	IF THE OBSERVER NO IS CORRECT THEN CALCULATIONS CAN BEGIN 90	J	86
C	IF NOT GO TO END OF DO-LOOP AND CONTINUE WITH LOOP	J	87
	IF (N-NORBS) 240,90,240		
90	CONTINUE	J	89
	CALL SECOND(CPTM)		
	IF(CPTM-180.)1722,1722,250		
1722	CONTINUE		
C	STORE RETARDED TIME IN T	J	91
	IN=IN+1	J	92
	T(IN)=F(J+1)	J	93
C	DEFINE TAU,DELTA TAU, AND ONE-HALF DELTA TAU	J	94
	TAU=F(J+1)/ROC	J	95
	DT=TAU-TPRM	J	96
	DEL=DT*.5	J	97
C	IS IT TIME TO CALL DOT	J	98
C	IF IT IS TIME GO TO 100		
	IF (CPTM-XT) 150,150,100		
100	CONTINUE	J	101
	XT=XT+XDOT	J	102
	ISTRT=ISTRT+1	J	103
C	PRINT RESTART GROUP NO. AND TIME POINT	J	104
	PRINT 410, ISTRT,T(IN)	J	105
C	CALL DOT(DUMP PROGRAM ON TAPE)	J	106
	CALL DOT (8)	J	107
C	THIS IS POINT 3	J	108
C	IS SENSE SWITCH 5 ON OR OFF	J	109
C	IF THE SS IS OFF CONTINUE AT 140	J	110
C	IF SS 5 IS ON GO TO 110 TO SPACE TAPES AND CONTINUE WITH CALC.	J	111
	IF (SENSE SWITCH 5)110,140	J	112
C	SPACE TAPES (PROGRAM HAS BEEN RESTARTED)	J	113
110	REWIND 1	J	114
	REWIND 2	J	115
	REWIND 4	J	116
	DO 120 IJL=1,IRCF	J	117
	READ (2) F	J	118
120	CONTINUE	J	119
	READ (2) FDUM	J	120
		J	121

	DO 130 IJL=1,IRCC	J	122
	READ (1) CK	J	123
	READ (4) R	J	124
130	CONTINUE	J	125
	CALL SECOND(CPTM)		
	XT=CPTM+XDUT		
C	PAUSE IN ORDER FOR SS 5 TO BE TURNED OFF	J	126
	PAUSE 5	J	127
140	CONTINUE	J	128
C	THIS IS POINT 3A	J	129
150	CONTINUE	J	130
	J=J+22		
	IP=0	J	132
	KN=0	J	133
	K7=0	J	134
	DO 210 KK=1,LLL	J	135
	KP=KZ	J	136
	L=2*KK-1	J	137
	XL=L	J	138
	FF=SQRT((2.*XL+1.)/(2.*XL*(XL+1.)))	J	139
C	SELECT ETHETA COEFF. FROM ARRAY READ FROM TAPE 2	J	140
C	MULT. COEFF. BY FACTOR IN ORDER FOR THEM TO BE COEFF OF NORMALIZED	J	141
C	ASSOCIATED LEGENDRE POLYNOMIALS	J	142
	R(KK)=F(J+KK-1)/FF	J	143
	DO 180 JJ=1,KK	J	144
	KZ=KZ+1	J	145
	PCEN(KZ)=CEN(KZ)	J	146
	XE=EXP(P(KZ)*DT)	J	147
	XA=P(KZ)*DT	J	148
C	IS DELTA TAU LARGE OR SMALL	J	149
C	IF LARGE GO TO 160 IF SMALL GO TO 170	J	150
	IF (D1*RR(KZ)-SM) 170,170,160	J	151
160	CONTINUE	J	152
C	DELTA TAU IS LARGE	J	153
C	USE SECOND SCHEME TO EVALUATE ICLN AND ISLN	J	154
	CEN(KZ)=XE*(CEN(KZ)*COS(XA)-SEN(KZ)*SIN(XA))	J	155
	R01=1./(RR(KZ)*RR(KZ))	J	156
	G=(R(KK)-BLAST(KK))/DT	J	157
	CEN(KZ)=CEN(KZ)-R01*((1.-XE+COS(XA))*(P(KZ)+BLAST(KK)+G*R01*PMQ(KZ	J	158
	1)) - XE*SIN(XA)*(BLAST(KK)*Q(KZ)+2.*G*PQ(KZ)*R01)+G*DT*P(KZ))	J	159
	SEN(KZ)=XE*(PCEN(KZ)*SIN(XA)+SEN(KZ)*COS(XA))+R01*((1.-XE+COS(XA))	J	160
	1*(Q(KZ)+BLAST(KK)+2.*G*PQ(KZ)*R01)+XE*SIN(XA)*(P(KZ)+BLAST(KK)+G*R	J	161
	201*PMQ(KZ))+G*DT*Q(KZ))	J	162
	GO TO 180	J	163
170	CONTINUE	J	164
C	DELTA TAU IS SMALL	J	165
C	USE TRAPIZODIAL METHOD TO EVALUATE ISLN AND ICLN	J	166
	CEN(KZ)=XE*((CEN(KZ)+DEL*BLAST(KK))*COS(XA)-SEN(KZ)*SIN(XA))+DEL*H	J	167
	1(KK)	J	168
	SEN(KZ)=XE*((PCEN(KZ)+DEL*BLAST(KK))*SIN(XA)+SEN(KZ)*COS(XA))	J	169
180	CONTINUE	J	170
	LMT=L+2	J	171
C	CALCULATE THE G QUANTITIES	J	172
	DO 200 K=1,LMT	J	173
	SUM=0.	J	174
	DO 190 N=1,KK	J	175
	K7=KN+1	J	176
	SUM=SUM+RK(KN)*((BETA(KP+N)*XS(KN)+GAMMA(KP+N)*XC(KN))*CEN(KP+N)+(J	177
	1)BETA(KP+N)*XC(KN)-GAMMA(KP+N)*XS(KN))*SEN(KP+N))	J	178
190	CONTINUE	J	179
C	THIS IS POINT 4	J	180
	IP=IP+1	J	181

	CA(IP)=SUM	J	182
200	CONTINUE	J	183
210	CONTINUE	J	184
	DO 220 IJ=1,20	J	185
	BDUM(IJ)=R(IJ)	J	186
220	BLAST(IJ)=R(IJ)	J	187
	DO 230 IJ=1,450	J	188
230	CKDM(IJ)=CK(IJ)	J	189
C	WRITE THE C QUANTITIES ON TAPE 1	J	190
	WRITE (1) CKDM	J	191
C	WRITE THE NORMALIZED COEFF. OF ETHETA ON TAPE 4	J	192
	WRITE (4) BDUM	J	193
	IRCC=IRCC+1	J	194
	IPR=TAU	J	195
C	THIS IS POINT 2A	J	196
C	HAVE 8 OBSERVER NOS. BEEN SCANNED	J	197
240	CONTINUE	J	198
C	IF YES THEN GO BACK TO 1A TO READ IN MORE COEFF	J	199
	GO TO 60		
C	THIS IS POINT 4A	J	201
250	LIMIT=IN-1	J	202
	WRITE (1) CKDM	J	203
	WRITE (4) BDUM	J	204
C	READ RUN NO. RADIUS, ANGLE OF EXTRAPOLATION	J	205
260	READ 400, NOBS, RL, ANG	J	206
	NVJ=(NORS/100)*100	J	207
	THETA=(ANG/180.)*PI	J	208
C	IS CARD BLANK	J	209
	IF (RL) 390,390,270	J	210
270	CONTINUE	J	211
	NJK=LLL*2+4	J	212
	RO=R/RL	J	213
	CALL LEG (NJK,PN,P1,THETA)	J	214
C	CALCULATE THE RATIO OF RADII TO THE J+1 POWER	J	215
	DO 280 I=1,NJK	J	216
280	ROR(I)=RO**I	J	217
	DO 281 I=1,6000		
281	RK(I)=0.		
	REWIND 1	J	218
	REWIND 2	J	219
	REWIND 4	J	220
	READ (4) BDUM	J	221
	READ (1) CKDM	J	222
C	CALCULATE EXTRAPOLATED ETHETA, ERADIAL, AND BPHI FOR EACH TIME PT.	J	223
	DO 340 IIJ=1,LIMIT	J	224
	IP=0	J	225
	KZ=0	J	226
	DO 290 IJL=1,450	J	227
290	CK(IJL)=CKDM(IJL)	J	228
	DO 300 IJL=1,20	J	229
300	B(IJL)=BDUM(IJL)	J	230
	READ (1) CKDM	J	231
	READ (4) BDUM	J	232
	SUM4=0.		
	SUM1=0.	J	233
	SUM2=0.	J	234
	SUM3=0.	J	235
	DO 330 M=1,LLL	J	236
	L=2*M-1	J	237
	L1=L+2	J	238
	IP=IP+L1	J	239
	SUM4=0.	J	240

	DO 130 IJL=1,IRCC	J	122
	READ (1) CK	J	123
	READ (4) R	J	124
130	CONTINUE	J	125
	CALL SECONJ(CPT4)		
	XT=CPT4*XDUT		
C	PAUSE IN ORDER FOR SS 5 TO BE TURNED OFF	J	126
	PAUSE 5	J	127
140	CONTINUE	J	128
C	THIS IS POINT 3A	J	129
150	CONTINUE	J	130
	J=J+22		
	IP=0	J	132
	KN=1	J	133
	K7=1	J	134
	DO 210 KK=1,LLL	J	135
	KP=KZ	J	136
	L=2*KK-1	J	137
	XL=L	J	138
	FF=SQRT((2.*XL+1.)/(2.*XL*(XL+1.)))	J	139
C	SELECT ETHETA COEFF. FROM ARRAY READ FROM TAPE 2	J	140
C	MULT. COEFF. BY FACTOR IN ORDER FOR THEM TO BE COEFF OF NORMALIZED	J	141
C	ASSOCIATED LEGENDRE POLYNOMIALS	J	142
	R(KK)=F(J+KK-1)/FF	J	143
	DO 180 JJ=1,KK	J	144
	KZ=KZ+1	J	145
	PCEN(KZ)=CEN(KZ)	J	146
	XE=EXP(P(KZ)*DT)	J	147
	XA=Q(KZ)*DT	J	148
C	IS DELTA TAU LARGE OR SMALL	J	149
C	IF LARGE GO TO 160 IF SMALL GO TO 170	J	150
	IF (D1*RR(KZ)-SM) 170,170,160	J	151
160	CONTINUE	J	152
C	DELTA TAU IS LARGE	J	153
C	USE SECOND SCHEME TO EVALUATE ICLN AND ISLN	J	154
	CEN(KZ)=XE*((CEN(KZ)*COS(XA)-SEN(K7)*SIN(XA))	J	155
	R01=1./(RR(KZ)*RR(KZ))	J	156
	G=(B(KK)-BLAST(KK))/DT	J	157
	CEN(KZ)=CEN(KZ)-R01*((1.-XE*COS(XA))*P(KZ)*BLAST(KK)+G*R01*PMQ(KZ)	J	158
	1))-XE*SIN(XA)*(BLAST(KK)*G(KZ)+2.*G*PQ(KZ)*R01)+G*DT*P(KZ))	J	159
	SEN(KZ)=XE*(PCEN(KZ)*SIN(XA)+SEN(KZ)*COS(XA))*R01*((1.-XE*COS(XA))	J	160
	1)*(Q(KZ)*BLAST(KK)+2.*G*PQ(KZ)*R01)+XE*SIN(XA)*(P(KZ)*BLAST(KK)+G*RJ	J	161
	201*PMQ(KZ))+G*DT*Q(KZ))	J	162
	GO TO 180	J	163
170	CONTINUE	J	164
C	DELTA TAU IS SMALL	J	165
C	USE TRAPIZODIAL METHOD TO EVALUATE ISLN AND ICLN	J	166
	CEN(KZ)=XE*((CEN(KZ)+DEL*BLAST(KK))*COS(XA)-SEN(KZ)*SIN(XA))+DEL*HJ	J	167
	1(KK)	J	168
	SEN(KZ)=XE*((PCEN(KZ)+DEL*BLAST(KK))*SIN(XA)+SEN(KZ)*COS(XA))	J	169
180	CONTINUE	J	170
	LMT=L+2	J	171
C	CALCULATE THE C QUANTITIES	J	172
	DO 200 K=1,LMT	J	173
	SJ1=0.	J	174
	DO 190 N=1,KK	J	175
	KP=K+1	J	176
	SJ1=SJ1+RK(KN)*((BETA(KP+N)*XS(KN)+GAMMA(KP+N)*XC(KN))*CEN(KP+N)+(J	J	177
	1)BETA(KP+N)*XC(KN)-GAMMA(KP+N)*XS(KN))*SFN(KP+N))	J	178
190	CONTINUE	J	179
C	THIS IS POINT 4	J	180
	IP=IP+1	J	181

	CK(IP)=SUM	J	182
200	CONTINUE	J	183
210	CONTINUE	J	184
	DO 220 IJ=1,20	J	185
	BDUM(IJ)=R(IJ)	J	186
220	BLAST(IJ)=H(IJ)	J	187
	DO 230 IJ=1,450	J	188
230	CKDM(IJ)=CK(IJ)	J	189
C	WRITE THE C QUANTITIES ON TAPE 1	J	190
	WRITE (1) CKDM	J	191
C	WRITE THE NORMALIZED COEFF. OF ETHETA ON TAPE 4	J	192
	WRITE (4) BDUM	J	193
	IRCC=IRCC+1	J	194
	IPR=TAU	J	195
C	THIS IS POINT 2A	J	196
C	HAVE 8 OBSERVER NOS. BEEN SCANNED	J	197
240	CONTINUE	J	198
C	IF YES THEN GO BACK TO 1A TO READ IN MORE COEFF	J	199
	GO TO 60		
C	THIS IS POINT 4A	J	201
250	LIMIT=IN-1	J	202
	WRITE (1) CKDM	J	203
	WRITE (4) BDUM	J	204
C	READ RUN NO, RADIUS, ANGLE OF EXTRAPOLATION	J	205
260	READ 400, NOBS, RL, ANG	J	206
	NVJ=(NORS/100)*100	J	207
	THETA=(ANG/180.)*PI	J	208
C	IS CARD BLANK	J	209
	IF (RL) 390,390,270	J	210
270	CONTINUE	J	211
	NJK=LLL*2+4	J	212
	RO=R/RL	J	213
	CALL LEG (NJK,PN,P1,THETA)	J	214
C	CALCULATE THE RATIO OF RADII TO THE J+1 POWER	J	215
	DO 280 I=1,NJK	J	216
280	ROR(I)=RO**(I)	J	217
	DO 281 I=1,6000		
281	RK(I)=0.		
	REWIND 1	J	218
	REWIND 2	J	219
	REWIND 4	J	220
	READ (4) BDUM	J	221
	READ (1) CKDM	J	222
C	CALCULATE EXTRAPOLATED ETHETA, ERADIAL, AND BPHI FOR EACH TIME PT.	J	223
	DO 340 IJL=1,LIMIT	J	224
	IP=0	J	225
	KZ=0	J	226
	DO 290 IJL=1,450	J	227
290	CK(IJL)=CKDM(IJL)	J	228
	DO 300 IJL=1,20	J	229
300	B(IJL)=RDUM(IJL)	J	230
	READ (1) CKDM	J	231
	READ (4) RDUM	J	232
	SUM4=0.		
	SUM1=0.	J	233
	SUM2=0.	J	234
	SUM3=0.	J	235
	DO 330 M=1,LLL	J	236
	L=2+M-1	J	237
	L1=L+2	J	238
	IP=IP+L1	J	239
	SUME=0.	J	240

	SUMR=0.	J	241
	SUMR=0.	J	242
	DO 320 JJ=1,L1	J	243
	L3=IP-JJ+1	J	244
	L4=IP-JJ	J	245
	KZ=KZ+1	J	246
	SUMF=SUME+V(KZ)*ROR(JJ)*CK(L3)	J	247
	IF (JJ-L1) 310,320,320	J	248
310	SUMR=J(KZ)*ROR(JJ+1)*CK(L4)+SUMR	J	249
	SUMR=J(KZ)*ROR(JJ)*CK(L3)+SUMR	J	250
	IF (RDJM) 320,320,311		
311	IF (JJ-1) 312,312,320		
312	SUMR=SUMF		
320	CONTINUE	J	251
	SUM1=SUM1-(SUMR*PN(L+1))*ZZ(M)	J	252
	SUM2=SUM2+RO*R(M)*P1(L+1)+SUME*P1(L+1)	J	253
	SUM3=SUM3+RO*B(M)*P1(L+1)+SUMR*P1(L+1)	J	254
	SUM4=SUM4+RO*R(M)*P1(L+1)+SUMRD*P1(L+1)		
330	CONTINUE	J	255
	IT=IJ+1	J	256
	E(IT)=SUM2/R	J	257
	EB(IT)=SUM3/(C*R)	J	258
	ER(IT)=SUM1	J	259
	RK(IT)=SUM4/R		
340	CONTINUE	J	260
	IF (RDJM) 345,345,341		
341	DO 342 ILM=1,IN,50		
	PRINT430 ,NNJ,PG		
	PRINT440,RL,ANG		
	PRINT450		
	MM=ILM+49		
	MJ=ILM		
	PRINT460,(T(IIK),RK(IIK),IIK=MJ,MM)		
450	FORMAT(1H0,36X*TIME*31X*RADIATION TERM*)		
460	FORMAT(1H ,31X2(E14.7,20X))		
342	CONTINUE		
	DO 371 KK=1,4		
	CALL GRAPH (KK,IN,4,4,10HLOCAL-TIME,10HRADIATION ,NNJ,T,RK,8.5,6.,		
	1.,0.)		
	CALL SYMBOL (6.6,.14,.14,8H(,0.,8)		
	CALL SYMBOL (7.56,.14,.14,6H, ,),0.,6)		
	CALL NUMBER (6.72,.14,.14,RL,0.,4HF6.0)		
	CALL NUMBER (7.68,.14,.14,ANG,0.,4HF3.0)		
371	CONTINUE		
C	PRINT AND PLOT THE FIELDS	J	261
345	CONTINUE		
	DO 350 ILM=1,IN,50	J	262
	CALL STPG (PG,NNJ,RL,ANG)	J	263
	MM=ILM+49	J	264
	MJ=ILM	J	265
	PRINT 420, (T(IIK),ER(IIK),F(IIK),EB(IIK),IIK=MJ,MM)	J	266
350	CONTINUE	J	267
	IF (IN-MM) 370,370,360	J	268
360	MM=-M+1	J	269
	CALL STPG (PG,NNJ,RL,ANG)	J	270
	PRINT 420, (T(IIK),ER(IIK),F(IIK),EB(IIK),IIK=MM,IN)	J	271
370	CONTINUE	J	272
	DO 380 KK=1,4	J	273
	CALL GRAPH (KK,IN,4,4,10HLOCAL-TIME,10HE-THETA ,NNJ,T,E,8.5,6.,3J	J	274
	1.,0.)	J	275
	CALL SYMBOL (6.6,.14,.14,8H(,0.,8)	J	276
	CALL SYMBOL (7.56,.14,.14,6H, ,),0.,6)	J	277

	CALL NUMBER (6.72,.14,.14,RL,0.,4HF6.0)	J	278
	CALL NUMBER (7.68,.14,.14,ANG,0.,4HF3.0)	J	279
	CALL GRAPH (KK,IN,4,4,10HLOCAL-TIME,10HF-R	,NNJ,T,ER,8.5,6.,J	280
	13.,0.)	J	281
	CALL SYMBOL (6.6,.14,.14,8H(.,0.,8)	J	282
	CALL SYMBOL (7.56,.14,.14,6H, .),0.,6)	J	283
	CALL NUMBER (6.72,.14,.14,RL,0.,4HF6.0)	J	284
	CALL NUMBER (7.68,.14,.14,ANG,0.,4HF3.0)	J	285
	CALL GRAPH (KK,IN,4,4,10HLOCAL-TIME,10HB-PHI	,NNJ,T,ER,8.5,6.,J	286
	13.,0.)	J	287
	CALL SYMBOL (6.6,.14,.14,8H(.,0.,8)	J	288
	CALL SYMBOL (7.56,.14,.14,6H, .),0.,6)	J	289
	CALL NUMBER (6.72,.14,.14,RL,0.,4HF6.0)	J	290
	CALL NUMBER (7.68,.14,.14,ANG,0.,4HF3.0)	J	291
380	CONTINUE	J	292
	CALL SECOND (OPTM)	J	293
	GO TO 260	J	295
390	CONTINUE	J	296
C	CARD WAS BLANK	J	297
C	TERMINATE THE PROGRAM	J	298
		J	299
400	FORMAT (110,2E10.3)		
410	FORMAT (1H ,*RESTART GROUP NO *15,* IS COMPLETE	LAST TIME POINT	
	1WAS*E10.3)		
420	FORMAT (1H ,31X4(E14.7,6X))	J	301
430	FORMAT (1H1,48X*RUN NUMBER*15,9X* . . . PAGE *F5.0,*.*)		
440	FORMAT (48X*(F6.0,*.,*F3.0,*.)*)		
	END	J	302-

	SUBROUTINE LEG (NN,P,P1,THETA)	J	1
	DIMENSION P(45), P1(45)	J	2
	DOUBLE PRECISION P,P1	J	3
	P(1)=1.	J	4
	P(2)=COS(THETA)	J	5
	DO 10 I=3,NN	J	6
	XN=I-2	J	7
	P(I)=((2.*XN+1.)*COS(THETA)*P(I-1)-XN*P(I-2))/(XN+1.)	J	8
10	CONTINUE	J	9
	N=NN-1	J	10
	DO 20 I=1,N	J	11
	XN=I	J	12
	P1(I)=XN*(COS(THETA)*P(I)-P(I+1))/SIN(THETA)	J	13
20	CONTINUE	J	14
	P(1)=P(1)*(0.5)**.5	J	15
	DO 30 I=2,N	J	16
	XN=I-1	J	17
	FACTN=SQRT((2.*XN+1.)/2.)	J	18
	FACT=SQRT((2.*XN+1.)/(2.*XN*(XN+1.)))	J	19
	P(I)=P(I)*FACTN	J	20
	P1(I)=P1(I)*FACT	J	21
30	CONTINUE	J	22
	RETURN	J	23
	END	J	24-

```

SUBROUTINE GREN (P,Q,BETA,GAMMA,PMQ,RR,THE,PQ,U,V)      J      1
DIMENSION U(500), V(500), P(220), Q(220), BETA(220), PJ  2
1MQ(220), PMQ(220), RR(220), THE(220)                J      3
DOUBLE PRECISION ZM,FY,UX,VX,FJ                       J      4
PI=3.141592653589793                                  J      5
KZ=0                                                    J      6
DO 30 I=1,20                                           J      7
L=I+2-1                                                J      8
M=(L+1)/2                                             J      9
KX=KZ+1                                               J     10
KY=KZ+M                                               J     11
READ 120, (P(KP),Q(KP),KP=KX,KY)                     J     12
DO 10 KP=KX,KY                                        J     13
READ 130, BETA(KP),GAMMA(KP)                          J     14
10 CONTINUE                                           J     15
DO 20 J=1,M                                           J     16
KZ=KZ+1                                               J     17
RR(KZ)=(P(KZ)*P(KZ)+Q(KZ)*Q(KZ))**.5                J     18
THE(KZ)=PI-ASIN(Q(KZ)/RR(KZ))                        J     19
PQ(KZ)=P(KZ)*Q(KZ)                                    J     20
PMQ(KZ)=P(KZ)*P(KZ)-Q(KZ)*Q(KZ)                    J     21
20 CONTINUE                                           J     22
30 CONTINUE                                           J     23
INIT=1                                                J     24
KZ=0                                                  J     25
DO 110 I=1,20                                         J     26
L=2+I-1                                              J     27
L1=L+1                                               J     28
L2=L+2                                               J     29
X=L                                                  J     30
DO 100 J=1,L2                                        J     31
Y=J                                                  J     32
ZM=1.                                                J     33
DO 40 K=1,J                                          J     34
SS=K                                                  J     35
ZM=ZM*(X+SS-1.)*(X-SS+2.)                          J     36
40 CONTINUE                                           J     37
IF (J-1) 50,50,60                                    J     38
50 FJ=1.                                              J     39
GO TO 70                                             J     40
60 FJ=FJ*(Y-1.)                                       J     41
70 CONTINUE                                           J     42
KZ=KZ+1                                               J     43
UX=ZM/(X*(X+1.)*FJ*2.**(J-1))                       J     44
U(KZ)=UX                                              J     45
IF (L-(J-1)) 80,90,90                               J     46
80 V(KZ)=V(KZ-1)                                     J     47
GO TO 100                                           J     48
90 CONTINUE                                           J     49
VX=U(KZ)*(X+(X+1.)+(Y-1.)*(Y-2.))/(X*(X+1.)-(Y-1.)*(Y-2.))
V(KZ)=VX                                             J     51
100 CONTINUE                                          J     52
110 CONTINUE                                          J     53
RETURN                                               J     54
C                                                    J     55
120 FORMAT (9XF13.0,7XF13.0)                        J     56
130 FORMAT (2E22.15)                                J     57
END                                                  J     58-

```


	SUBROUTINE STPG (PG,ING,RL,ANG)	J	1
	PRINT 10, ING,PG	J	2
	PRINT 20, RL,ANG	J	3
	PRINT 30	J	4
	PG=PG+1.	J	5
	RETURN	J	6
C		J	7
10	FORMAT (1H1,48X*KUN NUMBER*15,9X*. . . PAGE *F5.0,*.*)		
20	FORMAT (48X*(F6.0,*,*,F3.0,*,*)*)	J	9
30	FORMAT (1H0,36X*TIME*15X*ERADIAL*13X*ETHETA*15X*BPPI*)	J	10
	END	J	11-

```

SUBROUTINE DOT (NUM1)
DIMENSION L(1), NFILE(65), NFAD(65), NSSUBS(10)
DATA KRX,NSB,NSSUBS/1,9,3LDOT,6LIFENDF,5LGETBA,6LOUTPTB,6LINPUTR,4J
1LLOCF,4LXRCL,6LENDFIL,5LUMERR/
NUM=NUM1
GO TO (20,120,10), KRX
10 I=I*J*K*L*M*N*II*IJ*IK*IL*IM*IN*JI*JJ*JK*JL*JM*JN*KI*KJ*KK*KL*KM*KJ
I=A*B*C*D*E*F*G*H*O*P*Q*S*R*T*A*B*C*D*E*F*A*S*T*R*W*Q*X*Z*R*W*Y*I*GJ
I=I*J*K*L*M*N*II*IJ*IK*IL*IM*IN*JI*JJ*JK*JL*JM*JN*KI*KJ*KK*KL*KM*KJ
I=A*B*C*D*E*F*G*H*O*P*Q*S*R*T*A*B*C*D*E*F*A*S*T*R*W*Q*X*Z*R*W*Y*I*GJ
I=I*J*K*L*M*N*II*IJ*IK*IL*IM*IN*JI*JJ*JK*JL*JM*JN*KI*KJ*KK*KL*KM*KJ
I=A*B*C*D*E*F*G*H*O*P*Q*S*R*T*A*B*C*D*E*F*A*S*T*R*W*Q*X*Z*R*W*Y*I*GJ
I=I*J*K*L*M*N*II*IJ*IK*IL*IM*IN*JI*JJ*JK*JL*JM*JN*KI*KJ*KK*KL*KM*KJ
I=A*B*C*D*E*F*G*H*O*P*Q*S*R*T*A*B*C*D*E*F*A*S*T*R*W*Q*X*Z*R*W*Y*I*GJ
I=I*J*K*L*M*N*II*IJ*IK*IL*IM*IN*JI*JJ*JK*JL*JM*JN*KI*KJ*KK*KL*KM*KJ
20 KRX=2
LM=LOCF(L(1))-1
KK=0
DO 50 J=1,65
KK=KK+1
LOCAL=L(1+J-LM)
NAME=LOCAL.AND.7777777777777777000000B
IF (NAME.EQ.0) GO TO 60
NAME=LOCAL.AND.777777B
NFILE(KK)=L(NAME-LM).AND.7777777777777777000000B
NFAD(J)=NAME
JJ=J-1
IF (JJ.EQ.0) GO TO 50
DO 30 LMN=1,JJ
IF (NAME.EQ.NFAD(LMN)) GO TO 40
30 CONTINUE
NFAD(KK)=NAME
GO TO 50
40 KK=KK-1
50 CONTINUE
60 NF=KK-1
N=NF+1
ASSIGN 10 TO JK
JM=0
70 JK=JK-1
LOCAL=L(JK-LM).AND.7777777777777777000000B
IF (LOCAL.NE.NSSUBS(1)) GO TO 70
80 JQL=L(JK-LM).AND.777777B
JK=JK+JQL
IF (JM.EQ.NSB-1) GO TO 110
LOCAL=L(JK-LM).AND.7777777777777777000000B
DO 90 JJ=2,NSB
IF (LOCAL.EQ.NSSUBS(JJ)) GO TO 100
90 CONTINUE
GO TO 80
100 JM=JM+1
GO TO 80
110 LOCAL=JK
LAST=NFAD(NF)-1
LINEL=L(LAST+8-LM)
ASSIGN 130 TO KENT2
KFIELD=NFAD(1)
KFIELD=L(KFIELD-LM+4)
120 WRITE (NUM) LOCAL,KENT2,(L(I-LM),I=401,LOCAL),N,(L(I-LM),I=2,N)
WRITE (NUM) (L(I-LM),I=2,400),(L(I-LM),I=LOCAL,LAST)
END FILE NUM

```



```

SUBROUTINE GRAPH (IA, JM, IU, JC, IR, IL, IV, BR, AA, AP, BC, BS, AB)
COPYRIGHT 1966 CHRIS ASHLEY
DIMENSION BR(JM), AA(JM)
DATA JD, IC, IM, IW, RT, AC, AR, BE, JE, ID, CN, CO, BU, CQ, CF, CG, CH / -3, -2, 2, 10
1, 90, ., .07, .08, .14, 2HI9, 4HE8, ., .02, 1.32, .135, .33, .273704789, .6065102
263, .5278592375/
AS=0.
BF=0.
JF=1
IK=JM
IF (IK.LE.0.O.IK.GT.100000) IK=1
IF (IE.NE.3) GO TO 50
IF (IA.EQ.5) GO TO (300,530,460,530), IY
CALL PLOT (AS, BF, JD)
GO TO 60
50 CALL PLOT (IN, 0, 1)
IF (IV.EQ.0) GO TO 60
CALL REMARK (28H * FILMPL IS NOT DECLARED. *)
STOP 9
60 IE=3
AD=0.
AT=0.
IY=IA
IG=IU
IO=JC
IZ=IV
BV=AP
AE=RC
AJ=RS
BG=AB
JH=BV
AF=JH
IF (IY.LE.2) AU=0.
IF (IY.LT.1.O.IY.GT.4) IY=3
IF (IY.LE.1.O.IY.EQ.4) BG=0.
IF (IG.LT.1) IG=1
IF (IO.LT.1) IO=1
IF (BV.LE.0..O.BV.GT.8.95) BV=8.
IF (AE.LE.0..O.AE.GT.8.95) AE=8.
IF (IZ.GT.999999999) IZ=999999999
DO 70 JG=1, IK
AV=ABS(BR(JG))
BH=ABS(AA(JG))
70 IF (AD.LT.AV) AD=AV
IF (AT.LT.BH) AT=BH
IF (AD.LE.0.) AD=1.
IF (AT.LE.0.) AT=1.
JI=ALOG10(AD)
IH=ALOG10(AT)
IF (10.**JI.GT.AD) JI=JI-1
IF (10.**IH.GT.AT) IH=IH-1
GO TO (110,80,80,110), IY
80 IP=BG
BI=IP
HI=BG-BI
BW=BV-BG
II=RW
AW=II
BJ=BW-AW
JJ=IP+II
AG=BV-BJ

```

```

JN=JI-3
90 CI=10.**JN
DO 93 JN=1,9
CJ=JQ
93 IF(CJ*CI+RW.GE.AU)GO TO 97
JN=JN+1
GO TO 90
97 BX=CJ*CI
BK=RX*RW
CALL NUMBER (BI+CN,AU-BU,AC,(RI-BG)*BX,AH,ID)
CALL PLOT (AH,AU,IE)
CALL PLOT (RI,AU,IM)
CALL PLOT (RI,AU-.05,IM)
CALL PLOT (RI,AU,IM)
IQ=(RV+RG)*.5
DO 100 JA=1,JJ
RY=JA
AS=RY+RI
CALL PLOT (AS,AU,IM)
CALL PLOT (AS,AU-.05,IM)
CALL PLOT (AS,AU,IM)
IF (JA.LT.JJ) CALL NUMBER (AS-CF,AU-BU,AC,(AS-BG)*BX,AH,ID)
IF (JA.EQ.JJ) CALL NUMBER (AS-CG,AU-BU,AC,(AS-BG)*BX,AH,ID)
IF (JA.EQ.IQ) CALL SYMBOL ((BV+BG)*.5-CH,AU-CQ,RE,IB,AH,IW)
100 CALL PLOT (AS,AU,IE)
CALL PLOT (BV,AU,IM)
IF (IZ.NE.Q) CALL NUMBER (BV-CQ,AE*.05,RE,IZ,AH,JE)
CALL PLOT (BV,AH,IE)
GO TO (170,170,140,140),IY
110 AI=IG
JR=JI+1-IG
AY=JR
BL=10.**JR
CALL NUMBER (AH+CN,AU-BU,AC,BL,AH,ID)
CALL PLOT (AH,AU,IE)
BZ=BV/AI
AJ=-BZ
IQ=AI*.5
DO 130 IR=1,IG
BX=IR
AJ=AJ+BZ
DO 120 JA=1,10
BY=JA
BM=AJ+ALOG10(BY)*RZ
CALL PLOT (BM,AU,IM)
CALL PLOT (BM,AU-.05,IM)
120 CALL PLOT (BM,AU,IM)
IF (IR.LT.IG) CALL NUMBER (BM-CF,AU-BU,AC,10.**(JR+IR),AH,ID)
IF (IR.EQ.IG) CALL NUMBER (BM-CG,AU+BU,AC,10.**(JR+IG),AH,ID)
IF (IR.EQ.IQ) CALL SYMBOL (RV*.5-CH,AU-CQ,BE,IB,AH,IW)
130 CALL PLOT (BM,AU,IE)
IF (IZ.NE.Q) CALL NUMBER (BV-CQ,AE*.05,RE,IZ,AH,JE)
CALL PLOT (BV,AH,IE)
GO TO (170,170,140,140),IY
140 JK=AU
AK=JK
AK=AU-AK
AZ=AE-AU
JB=AZ
CB=JB
AL=AZ-CB
IS=JK+JB

```

```

BN=AE-AL
CK=AE-AIJ
JP=IH-3
150 CL=10.**JP
DO 153 JQ=1,9
CM=JQ
153 IF(CM*CL*CK.GE.AT) GO TO 157
JP=JP+1
GO TO 150
157 BB=CM*GL
AM=BB*BW
CALL PLOT (BV,AK,IM)
CALL PLOT (BV+.05,AK,IM)
CALL PLOT (BV,AK,IM)
DO 160 JA=1,IS
BY=JA
BF=BY+AK
CALL PLOT (BV,BF,IM)
CALL PLOT (BV+.05,BF,IM)
160 CALL PLOT (BV,BF,IM)
CALL PLOT (BV,AE,IM)
GO TO (220,200,200,220),IY
170 BA=IO
JS=IH+1
BO=JS-IO
CD=10.**BO
AN=AE/BA
AJ=-AN
DO 190 IR=1,IO
AJ=AJ+AN
DO 190 JA=1,10
BY=JA
BM=AJ+ALOG10(BY)*AN
CALL PLOT (BV,BM,IM)
CALL PLOT (BV+.05,BM,IM)
190 CALL PLOT (BV,BM,IM)
GO TO (220,200,200,220),IY
200 CALL PLOT (AG,AE,IM)
CALL PLOT (AG,AE+.05,IM)
CALL PLOT (AG,AE,IM)
DO 210 JA=1,JJ
BY=JA
AS=AG-BY
CALL PLOT (AS,AE,IM)
CALL PLOT (AS,AE+.05,IM)
210 CALL PLOT (AS,AE,IM)
CALL PLOT (AH,AE,IM)
CALL PLOT (BG,AE,IE)
GO TO (270,270,250,250),IY
220 CALL PLOT (BV,AE+.05,IM)
CALL PLOT (BV,AE,IM)
AJ=BV+BZ
DO 240 IR=1,IG
AJ=AJ-BZ
DO 240 JA=1,10
BY=11-JA
BM=AJ-BZ+ALOG10(BY)*BZ
CALL PLOT (BM,AE,IM)
CALL PLOT (BM,AE+.05,IM)
240 CALL PLOT (BM,AE,IM)
GO TO (270,270,250,250),IY
250 IQ=CK*.5

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```

CALL PLOT (RG,BN,IM)
CALL PLOT (RG-.05,BN,IM)
CALL PLOT (RG,BN,IM)
CALL NUMBER (RG-BU,BN-CG,AC,CR*RB,RT,ID)
CALL PLOT (RG,BN,IF)
DO 260 JA=1,IS
BY=JA
BF=BN-BY
CALL PLOT (RG,BF,IM)
CALL PLOT (RG-.05,BF,IM)
CALL PLOT (RG,BF,IM)
IF (JA,LT.IS) CALL NUMBER (RG-BU,BF-CF,AC,(BF-AU)*BB,RT,ID)
IF (JA,EQ.IS) CALL NUMBER (RG-BU,BF*CN,AC,(BF-AU)*BB,RT,ID)
IF (JA,EQ.IQ) CALL SYMBOL (RG-CQ,(AF*AU)*.5*CH,RE,IL,RT,IW)
260 CALL PLOT (RG,BF,IE)
CALL PLOT (RG,AN,IM)
GO TO (300,530,460,530),IY
270 CALL PLOT (RG-.05,AE,IM)
CALL PLOT (RG,AE,IM)
AJ=AE+AN
IQ=RA*.5
CALL NUMBER (RG-BU,AE-CG,AC,10.**JS,RT,ID)
CALL PLOT (RG,AE,IE)
DO 290 IR=1,IQ
AJ=AJ-AN
DO 280 JA=1,10
BY=11-JA
BM=AJ-AN+ALOG10(BY)*AN
CALL PLOT (RG,BM,IM)
CALL PLOT (RG-.05,BM,IM)
280 CALL PLOT (RG,BM,IM)
IF (IR,LT.IQ) CALL NUMBER (RG-BU,BM-CF,AC,10.***(JS-IR),BT,ID)
IF (IR,EQ.IQ) CALL NUMBER (RG-BU,BM*CN,AC,10.***(JS-IR),BT,ID)
IF (IR,EQ.IQ) CALL SYMBOL (RG-CQ,AE*.5*CH,BE,IL,BT,IW)
290 CALL PLOT (RG,BM,IE)
GO TO (300,530,460,530),IY
300 DO 450 JG=1,IK
BP=AS
CE=BF
IJ=1
IF (BR(JG),LT.BL) IJ=3
IF (AA(JG),LT.CD) IJ=IJ+1
GO TO (430,310,390,410),IJ
310 IF (AA(JG),GT.-CD) GO TO 350
IT=1
AS=(ALOG10(BR(JG))-AY)*BZ
320 BF=(ALOG10(-AA(JG))-BO)*AN
330 IF (JF,EQ.3) GO TO 340
JF=3
GO TO 380
340 RQ=RQ+SQRT((AS-BP)**2+(BF-CE)**2)
IF (BQ,LT..5) GO TO 440
BQ=C.
IF (AS,GT.BV) AS=BV
IF (BF,GT.AE) BF=AE
CALL SYMBOL (AS,BF,AR,IT,AH,IC)
GO TO 450
350 AS=(ALOG10(BR(JG))-AY)*BZ
360 BF=C.
370 JF=1
380 IF (AS,GT.BV) AS=BV
IF (BF,GT.AE) BF=AE

```

```

CALL PLOT (AS,BF,IE)
GO TO 450
390 IF (BR(JG).GT.-RL) GO TO 400
    IT=9
    AS=(ALOG10(-BR(JG))-AY)*BZ
    BF=(ALOG10(AA(JG))-RO)*AN
    GO TO 330
400 AS=0.
    BF=(ALOG10(AA(JG))-RO)*AN
    GO TO 370
410 IF (BR(JG).GT.-RL.O,AA(JG).GT.-CD) GO TO 420
    IT=2
    AS=(ALOG10(-BR(JG))-AY)*BZ
    GO TO 320
420 AS=0.
    GO TO 360
430 AS=(ALOG10(BR(JG))-AY)*BZ
    BF=(ALOG10(AA(JG))-RO)*AN
    IF (JF.EQ.2) GO TO 440
    JF=2
    GO TO 380
440 IF (AS.GT.BV) AS=BV
    IF (BF.GT.AE) BF=AE
    CALL PLOT (AS,BF,IM)
450 CONTINUE
    RET IRV
460 DO 520 JG=1,IK
    AS=BR(JG)/BX+RG
    BF=AA(JG)/BB+AU
    IJ=1
    IF (AS.LT.0) IJ=3
    IF (BF.LT.0) IJ=IJ+1
    GO TO (470,500,480,490),IJ
470 IF (JG.EQ.1) GO TO 510
    IF (AS.GT.BV) AS=BV
    IF (BF.GT.AE) BF=AE
    CALL PLOT (AS,BF,IM)
    GO TO 520
480 AS=0.
    GO TO 510
490 AS=0.
500 BF=0.
510 IF (AS.GT.BV) AS=BV
    IF (BF.GT.AE) BF=AE
    CALL PLOT (AS,BF,IE)
520 CONTINUE
    RETURN
530 IT=1
    IF (IY.EQ.2) GO TO 540
    BX=BB
    BO=AY
    AN=BZ
    CD=RL
    BG=AU
    IT=9
540 JL=IT
    DO 660 JG=1,IK
    BP=AS
    CE=BF
    IF (IY.NE.4) GO TO 550
    AO=BR(JG)
    BR(JG)=AA(JG)

```



```

AA(JG)=A0
550 AS=BR(JG)/BX+RG
    IF (AS.GE.0.) GO TO 560
    AS=0.
    JF=1
560 IF (AA(JG).GT.CD) GO TO 620
    IF (AA(JG).GT.-CD) GO TO 590
    RF=(ALOG10(-AA(JG))-B0)*AN
    IF (IY.NE.4) GO TO 570
    A0=AS
    AS=RF
    BF=A0
570 IF (JF.EQ.3) GO TO 580
    JF=3
    GO TO 610
580 B0=B0+SQRT((AS-RP)**2+(RF-CF)**2)
    IF (B0.LT..5) GO TO 640
    B0=.
    IF (AS.LT.BG.0.RF.LT.AU) IT=2
    IF (AS.GT.BV) AS=BV
    IF (RF.GT.AE) BF=AE
    CALL SYMBOL (AS,BF,AR,IT,AH,IC)
    IT=UL
    GO TO 650
590 BF=R.
    IF (IY.NE.4) GO TO 600
    A0=AS
    AS=RF
    BF=A0
600 JF=1
610 IF (AS.GT.BV) AS=BV
    IF (RF.GT.AE) BF=AE
    CALL PLOT (AS,BF,IF)
    GO TO 650
620 BF=(ALOG10(AA(JG))-B0)*AN
    IF (IY.NE.4) GO TO 630
    A0=AS
    AS=RF
    BF=A0
630 IF (JF.EQ.2) GO TO 640
    JF=2
    GO TO 610
640 IF (AS.GT.BV) AS=BV
    IF (RF.GT.AE) BF=AE
    CALL PLOT (AS,BF,IM)
650 IF (IY.NE.4) GO TO 660
    A0=BR(JG)
    BR(JG)=AA(JG)
    AA(JG)=A0
560 CONTINUE
    RETURN
    END

```



```
SUBROUTINE NUMBER(X,Y,HT,FNUM,ROT,FORMAT)
DIMENSION FORM(3),TEMP(3)
ISIZE=7
IF (HT.LT.(.220450)) ISIZE=6
IF (HT.LT.(.155525)) ISIZE=5
IF (HT.LT.(.110375)) ISIZE=4
CALL PLOT (X,Y,3)
IOR=0
IF(ROT.GT.45)IOR=1
FORM(1)=1H(
FORM(2)=FORMAT
FORM(3)=1H)
ENCODE(.30,FORM,TEMP)FNUM
CALL PLOT (TEMP(1),IOR,ISIZE)
RETURN
END
```

